# A Novel Approach to Quantify Air-Water Gas Exchange in Shallow Surface Waters Using High-Resolution Time Series of Dissolved Atmospheric Gases

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2 Abstract

Gas exchange across the air-water interface is a key process determining the release of greenhouse gases from surface waters, and a fundamental component of gas dynamics

in aquatic systems. In order to experimentally quantify the gas transfer velocity in a wide range of aquatic settings, a novel method is presented based on recently developed techniques for the *in situ*, near-continuous measurement of dissolved (noble) gases with a field-portable mass spectrometer.

Variations in observed dissolved gas concentrations are damped and lagged with respect to equilibrium concentrations, being the result of (a) temperature (and thus solubility) variations, (b) water depth and (c) the specific gas transfer velocity  $(k_i)$ . The method fits a model to the measured gas concentrations to derive the gas transfer velocity from the amplitude and the phase lag between observed and equilibrium concentrations. With the current experimental setup, the method is sensitive to gas transfer velocities of  $0.05 - 9 \, m/d$  (for  $N_2$ ), at a water depth of  $1 \, m$ , and a given daily water temperature variation of  $10 \, ^{\circ}C$ . Experiments were carried out (a) in a controlled experiment to prove the concept and to confirm the capability to determine low transfer velocities and (b) in a field study in a shallow coastal lagoon covering a range of transfer velocities, demonstrating the field applicability of the method.

# 20 Introduction

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Gas exchange across the air-water interface is a key process coupling atmospheric and aquatic gas cycles. Accurate knowledge of gas exchange rates is required to determine mass balances of dissolved gases in aquatic systems, which can in turn be used to estimate fluxes between 23 groundwater reservoirs and surface water. 1-3 Surface water bodies can be sources or sinks for 24 gases: 4,5 whereas release of methane and carbon dioxide from water bodies is an important 25 source of greenhouse gases to the atmosphere, the reverse flux of oxygen and nitrogen from 26 atmosphere to water is an important factor in water quality and ecosystem functioning.<sup>6</sup> 27 The gas transfer velocity for open ocean conditions is well parametrized in its dependence 28 on wind speed. Furthermore, numerous empirical relationships are available for rivers where 29 gas exchange is primarily a function of turbulent mixing due to water flow. 8 In contrast, for shallow open water surfaces like shallow lakes and, importantly, the coastal zone of oceans, a
parametrization is currently not available that fully takes into account the physical processes
driving gas exchange, which differ significantly from those in the open ocean or rivers. In
these systems, the influence of other environmental parameters, e.g. rain, 9,10 current velocity
or bottom roughness, on near surface turbulence increases due to the decreased wind fetch
and lower water depth. 11 and this fundamentally impacts air/water partitioning.

A commonly used method for estimating the transfer velocity at specific sites over short time scales consists of injecting and monitoring trace gases. <sup>11–14</sup> Besides being experimentally demanding <sup>11</sup> and sometimes being subject to environmental regulation (e.g. SF<sub>6</sub>), trace gas injection may contaminate the sites and render future experiments impossible. <sup>15</sup>

Recently, in studies primarily targeting the estimation of residence times of water within catchments, it was noted that diurnal variations in water temperature in rivers produced periodically varying concentrations of dissolved gases, which were damped and lagged in comparison with atmospheric equilibrium concentrations.<sup>15</sup>

Variations of the gas concentrations are a function of the temperature variation, the temperature-dependence of gas solubility in water, and the gas transfer velocity. In principle, synchronous measurement of time series of temperature and concentrations of dissolved gases therefore allows the gas transfer velocity to be estimated. Recent advances in determining gas concentrations have led to the development of field portable MIMS (membrane inlet mass spectrometry) systems that can measure concentrations of He, Ar, Kr, N<sub>2</sub>, O<sub>2</sub>, CO<sub>2</sub> and CH<sub>4</sub> with relatively high accuracy and precision. These novel techniques allow insitu, real-time measurement of gas concentration time series with a temporal resolution of a few minutes and make subsequent laboratory analysis redundant.

The objective of this study is to combine the approach to calculate gas exchange rates <sup>15</sup> with those novel measurement techniques. Further, we aim to establish the environmental conditions for which gas transfer velocities can be derived using the diurnal gas dynamics (DGD). We first calculate the sensitivity and resolution of the presented method in a theo-

retical setting. The performance and the experimental requirements are then demonstrated in a controlled experiment and in the large, shallow La Palme lagoon at the Mediterranean 59 Sea in southern France. 60

### Theory 61

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The gas flux of species i between air and water is caused by a disequilibrium of aquatic and 62 atmospheric gas concentrations: 19 63

$$F_i = k_i \cdot \Delta C_i = k_i \cdot (C_{w,i} - C_{eq,i}), \tag{1}$$

with  $F_i$  being the gas flux,  $C_{w,i}$  the concentration in the water, and  $C_{eq,i}$  the concentration in air saturated water, and  $k_i$  is the gas transfer velocity, which reflects the rate of exchange. This basic relation, even though not accounting for bubble-mediated gas fluxes, is used to determine fluxes at regional-to-global scales.<sup>7</sup> 67 If the water is well mixed, the flux can also be written as

$$F_i = \frac{dC_{w,i}}{dt} \cdot h,\tag{2}$$

with h being the water depth of the exchanging water mass ('mixed layer'). Equating 1 and 2 yields

$$\frac{dC_{w,i}}{dt} = \frac{k_i}{h} \cdot (C_{w,i} - C_{eq,i}). \tag{3}$$

The equilibrium gas concentrations depend on the temperature  $(T_w)$  and the salinity (S)71 of the water and the partial pressure of each gas, and are determined by Henry's law, 20

$$C_{eq,i} = \frac{p_i}{H_i(T_w, S)}. (4)$$

The Henry's coefficient  $(H_i)$  is specific to each gas species.  $^{21-23}$   $p_i$  is the partial pressure of

species i in the atmosphere and is given by  $p_i = (p_{atm} - e_s(T_w))v_i$ , with  $p_{atm}$  the local total atmospheric pressure,  $e_s(T_w)$  the water vapor pressure, and  $v_i$  the volume fraction of gas i in dry air.<sup>20</sup>

Diurnal variation in  $C_{eq,i}$  for the different gases is largely a function of the temperature dependence of their solubilities. The magnitude of the diurnal variation in  $C_{eq,i}$  for the noble gases will therefore be greatest for Xe and Kr, less for Ar and least for He and Ne.

The temperature dependence of the solubility of  $N_2$  is similar to that of Ar.

To convert the transfer velocity derived from one gas species to another commonly the respective Schmidt numbers are used. The Schmidt number is defined as the ratio of kinematic viscosity of water, divided by the diffusion coefficient of the gas in water. The transfer velocities  $(k_{1,2})$  of gas 1 and 2 are linked to each other via their Schmidt numbers  $(Sc_{1,2})$  in a power law dependence with the Schmidt number exponent (n):

$$\frac{k_1}{k_2} = \left(\frac{Sc_1}{Sc_2}\right)^{-n} \tag{5}$$

where n theoretically ranges from 1/2 < n < 2/3. However, n decreases rapidly to 1/2 with the onset of waves  $^{24}$  (free surface condition). The ratio of  $(Sc_1/Sc_2)$  is approximately constant with temperature.  $^{25}$ 

While concentration gradients for reactive gases can also occur due to biogeochemical reactions, i.e. photosynthetic production in the case of O<sub>2</sub> and production by denitrification in the case of N<sub>2</sub>, the concentrations of the (atmospheric) noble gases are only controlled by physical processes, specifically radioactive decay and air-water gas-exchange.

# 93 Method

### 94 Modeling

- An ordinary differential equation solver is used to derive the results for the expected in-situ
- concentrations  $(C_{w,i})$  by solving Eq. 3. The mean of the first ten measured  $C_{w,i}$  of a time
- 97 series is used as the initial gas concentration.
- The parameters for the equilibrium concentrations  $(C_{eq,i})$  (cf. Eq. 4) and the water
- depth are given by the local environmental system, so that the transfer velocity  $(k_i)$  and
- $C_{w,i}$  remain as the only free parameters.
- The model is fit to the measured concentrations by varying  $k_i$ . The fit is optimized by
- minimizing the sum of squared errors (SSE) between the measured and modeled concentra-
- tions of the respective gas species.
- The uncertainty of the best-fit gas exchange rate  $k_i^*$  (95% confidence interval) was deter-
- mined from the scatter of the observed concentrations relative to the best-fit model curves. <sup>26</sup>
- The measured gas concentrations time series of the field study were filtered with a Savitzky-
- Golay filter (order 3, frame length 21) to reduce noise. <sup>27</sup>

## 108 Experimental Method

- The concentrations of dissolved  $N_2$ ,  $^{40}{\rm Ar}$  and  $^{84}{\rm Kr}$  in the water were analyzed with a
- portable 'miniRUEDI' mass spectrometer <sup>16</sup> (Gasometrix GmbH) using the gas-equilibrium
- membrane-inlet mass spectrometry method (GE-MIMS). 16,28,29 For later calculations 40 Ar
- $^{112}$  and  $^{84}\mathrm{Kr}$  are converted to elemental concentration.  $^{20}$
- During the experiments a submersible pump was used to continuously sample the water
- through a membrane contactor module (Liqui-Cel G542), in which the gases equilibrate
- between the water and a small gas headspace according to Henry's law. The partial pressures
- $^{116}$  of  $\mathrm{N_2},\,^{40}\mathrm{Ar}$  and  $^{84}\mathrm{Kr}$  in the headspace were quantified from the mass spectrometer readings
- by peak-height comparison relative to analyses of ambient air, which was used as calibration

standard.<sup>16</sup> The analytical sequence was a continuously repeating cycle consisting of one air-standard analysis block, followed by three water sample analysis blocks, followed by one ambient air sample analysis block to assess the analytical performance.<sup>16</sup> Each of these analysis blocks were 8 *min* long.

The partial pressures observed in the headspaces of the membrane modules were converted to dissolved gas concentrations using the gas-specific Henry's law coefficients at the temperature of the water in the membrane modules. The partial pressures obtained from the ambient-air samples were used to estimate the analytical uncertainties of the dissolved-gas concentrations as 1% for  $N_2$ , 2.5% for Ar and 4% for Kr.

In the controlled experiment and the field study at La Palme lagoon, in-situ water temperature, salinity and atmospheric pressure were recorded by sensors every  $10 \, min$  in order to calculate  $C_{eq,i}$  using Eq. 4.

### 130 Controlled Experiment

A concept test of the DGD method to determine gas transfer velocities was conducted outside the Swiss Federal Institute of Aquatic Science and Technology (Eawag) in Dübendorf, Switzerland. For that purpose, a small tank ( $height = 15 \, cm$ ,  $length = 60 \, cm$ ,  $width = 40 \, cm$ ) with a black shell was used. The small volume (0.036  $m^3$ ) and the black color of the tank caused a large temperature increase of the water in response to sun irradiation and a rapid decline in water temperature as air temperature dropped at night.

The water in the tub was circulated through the membrane module, where the gases equilibrate for measurement. Cavitation was not observed with a pumping rate of about 2l/min. The forced circulation caused an increase in turbulence in the water, producing a well mixed water body. This turbulence is assumed to be constant over time, as the pumping rate was kept constant. The development of (breaking) waves was heavily suppressed by the walls and the small surface area of the tank.

### 143 Field Study at La Palme Lagoon

The DGD method was further applied during a field campaign in June 2017 at La Palme lagoon on the French coastline of the Mediterranean Sea. The shallow lagoon has a surface area of approximately  $5 \, km^2$ , a mean depth of  $0.6 \, m$  and a maximum depth of  $1.8 \, m$ . The water level was not influenced by tides, as there was no direct hydraulic connection of the lagoon to the sea.

The small depth of the lagoon ensures the water heats up quickly in response to solar irra-149 diation and loses heat quickly at night, which leads to large diurnal temperature variations. 150 The lagoon is regularly exposed to strong north-westerly winds, which cause waves of a max-151 imum amplitude of about  $0.4 \, m.^1$  Inflow of groundwater occurs in the northern section of the 152 lagoon. 1 Recirculation of water between the lagoon and the pore space of shallow sediments 153 is considerable and flows vary with up to an order of magnitude. 1,30 Such water exchange 154 might influence the concentrations of some of the gases. <sup>31</sup> Particularly, He being enriched in 155 the pore water of sediments by in-situ production or groundwater input might be subject to 156 variations in the mixing of the water masses. Further, can O<sub>2</sub> be significantly consumed by 157 the sediments. However, Ar and Kr are not affected by sediment/water exchange. 32 158

The gas measurements were carried out near the center of the lagoon. Water was pumped 159 55 m from the sampling point at a water depth of 1 m to the onshore GE-MIMS system 160 by a submersible pump through a hard plastic tube (polyamide tubing; 66 m in length). 161 Cavitation was not observed during the course of the experiments and phase separation does 162 not result in systematic errors as long as the travelling time of both phases is the same. 163 Mechanical filters and regular cleaning of the membrane contactors kept the flow rates high 164 to guarantee reliable gas measurements. The travel time of the water through the hoses was 165 estimated to be approximately 5 min which is negligibly small in comparison to the diurnal 166 variation. 167

### 168 Results and Discussion

### 169 Resolution and Sensitivity

The DGD method allows determination of gas exchange rates only within a certain range of k/h values. Here we discuss the upper and lower limits of the determination of the transfer velocity using the DGD approach, and elaborate on the constraining parameters.

We have run the model several times in a theoretical setting to determine the sensitivity and resolution of the method. For that purpose a synthetic sinusoidal variation in the water temperature simulate the diurnal heating and cooling. This pre-set temperature cycle has a mean temperature value of  $15\,^{\circ}C$ , a peak-to-peak amplitude of  $2\,^{\circ}C$ ,  $6\,^{\circ}C$ ,  $10\,^{\circ}C$ ,  $16\,^{\circ}C$  or  $20\,^{\circ}C$  and a  $24\,h$  period.  $C_{eq,i}$  were calculated for a constant atmospheric pressure of  $1013.15\,hPa$ . The expected water concentrations  $C_{w,i}$  are modeled for a k/h-range of  $0-10\,d^{-1}$ .

This synthetic data exercise allow us to derive upper and lower bounds for the deter-180 mination of the gas transfer velocities by comparing the parameters to the experimental 181 precision of the gas measurements. We define two quantities necessary to be resolved by 182 the measurement setup.  $(D_i)$  is the maximum difference between the expected water con-183 centration and the equilibrium concentration normalized to the mean equilibrium concen-184 tration of one period,  $D_i = \frac{max(|C_{w,i}(t) - C_{eq,i}(t)|)}{\overline{C_{eq,i}}}$ . We define  $(A_i)$  as the amplitude of the 185 expected concentration normalized to the mean equilibrium concentration of the time series 186  $A_i = \frac{\max(C_{w,i}(t)) - \min(C_{w,i}(t))}{\overline{C_{eq,i}}}.$ 187

For very low k/h,  $C_{w,i}$  approaches a constant value. The water concentrations will be approximately equal to the equilibrium concentration at the daily mean water temperature. The lower limit of resolution of k/h is shown in Fig. 1 for Ar and for the five different values of diurnal water temperature variation. In this case, the experimental setup is not sensitive to changes in k/h as the amplitude,  $A_{Ar}$  (yellow, right y-axis), due to temperature becomes less than the analytical precision (red line in Fig. 1; for Ar) of the gas measurements.

The limit is higher for lower diurnal temperature differences as the concentration gradients are smaller. For a water temperature amplitude of  $10\,^{\circ}C$  the lower limit is approximately 0.07  $d^{-1}$  for Ar,  $0.05\,d^{-1}$  for N<sub>2</sub> and  $0.1\,d^{-1}$  for Kr. The smaller the temperature amplitude of the daily forcing the higher the minimum of k/h that can be reliably determined.

For high k/h, the gas concentrations in surface water rapidly approaches  $C_{eq,i}$ , such 198 that the difference between  $C_{w,i}$  and  $C_{eq,i}$  gets small. Any further increase in k/h will not 199 produce detectable changes between the expected and the equilibrium concentration, leaving 200 the method insensitive for large k/h. Fig. 1 shows  $D_{Ar}$  (blue, left y-axis). The upper limit of 201 the method is the point at which the difference between the expected concentration and the 202 equilibrium concentration becomes smaller than the analytical precision. The upper limit 203 of the method is, therefore, reached if  $D_{Ar}$  is smaller than the analytical precision. For a 204 diurnal temperature change of  $10^{\circ}C$ , the upper limit of k/h that can be reliably measured 205 is approximately  $4 d^{-1}$  for Ar,  $9 d^{-1}$  for N<sub>2</sub> and  $2 d^{-1}$  for Kr. The smaller the temperature 206 amplitude the lower the maximum of k/h that can be reliably determined. 207

The range of k/h values that can be reliably determined by Ar is therefore approximately  $0.07 - 4 d^{-1}$  for a diurnal temperature variation of  $10 \,^{\circ}C$ . Results for water depths of  $0.2 \, m$  and  $0.6 \, m$  are of  $0.01 - 0.8 \, m/d$  and  $0.04 - 2.4 \, m/d$ , respectively.

The ability to resolve differences in gas transfer velocity therefore depends on the magnitude of diurnal water temperature variation, on the water depth, on the temperature dependence of the solubility in water and on the measurement precision. The latter two factors are specific to each gas species.

In summary, the range of gas transfer velocities that can be determined by the DGD method falls well in the range of gas transfer velocities that are typically encountered in natural waters (average for lakes and reservoirs  $1.0 \, m/d$ ; global average  $5.7 \, m/d$ ).

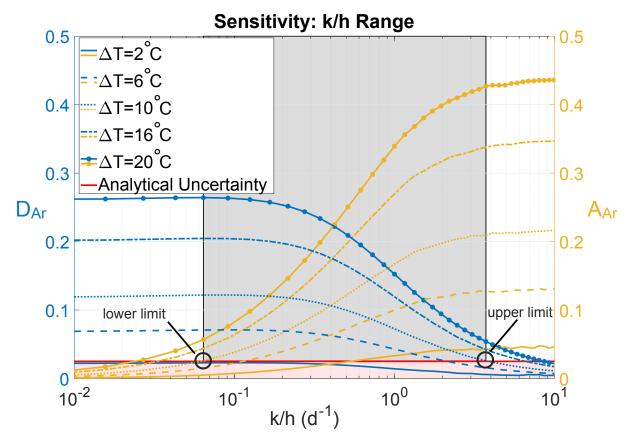


Figure 1: The maximal concentration difference between expected concentration in water and equilibrium concentration  $(D_{Ar})$  (blue, left y-axis) and the amplitude of the water concentration  $(A_{Ar})$  (yellow, right y-axis) both normalized to the mean equilibrium concentration shown for different water temperature amplitudes. High k/h results in a small difference between the expected and equilibrium concentrations, hence, small  $D_{Ar}$ . Where  $D_{Ar}$  is less than the experimental precision (that for Ar is indicated by the red horizontal line),  $C_{eq,i}$  and  $C_{w,i}$  cannot be reliably differentiated, determining the upper limit on the k/h range. At low k/h the expected diurnal concentration amplitude,  $A_{Ar}$ , is less than the experimental precision. This, therefore, defines the lower limit for k/h determination. The range for  $\Delta T = 10^{\circ}C$  (grey area and black circles) is approximately  $0.07 - 4 d^{-1}$  for Ar with an experimental uncertainty of 2.5%.

### 218 Controlled Experiment

The results of the equilibrium, the observed and the modeled gas concentrations for  $N_2$ , Ar 219 and Kr in the controlled experiment are shown in Fig. 2. The large diurnal amplitude in 220 water temperature in the tub (up to  $25\,^{\circ}C$ ) result in large variations in  $C_{eq,i}$ . The observed 221  $C_{w,i}$  are lagged and their amplitudes are damped relative to  $C_{eq,i}$ , as predicted by the model. 222 Concentration changes in the dissolved gas concentrations are as high as 45% for Kr, 16%223 for Ar and 13% for  $N_2$  relative to the lowest measured concentration. These changes are the 224 direct result of the different solubilities and the analytical uncertainties. 225 The model reproduces the measured concentrations for the gases very well. The best-fit 226 gas exchange rates are:  $k_{Ar}^* = 0.29 \pm 0.01 \, m/d, \, k_{N_2}^* = 0.27 \pm 0.02 \, m/d, \, k_{Kr}^* = 0.39 \pm 0.06 \, m/d.$ 227 Those values result in a ratio of  $k_{N_2}^*/k_{Ar}^* = 0.93 \pm 0.02$ , which is, within the uncertainty, the 228 same as the expected value of 0.95 from Eq. 5 (Schmidt numbers for fresh water at  $T=20\,^{\circ}C$ : 229  $Sc_{Ar} = 552$ ,  $Sc_{N_2} = 612$ ,  $Sc_{Kr} = 625$ <sup>7</sup>). For Kr the derived solution of the transfer velocity 230 matches with that scaled from Ar with the Schmidt number ratio  $(k_{SC,Kr} = 0.27 \, m/d)$  within 231 its  $2\sigma$  confidence interval.  $k_{SC,Kr}$  also fits the data well given the scattering of the data (Fig. 232 2). Due to the lower experimental precision the error of the estimated gas transfer velocity 233 is larger for Kr than for Ar and  $N_2$ . To illustrate the ability of the DGD method to reproduce  $C_{w,i}$ , model results for N<sub>2</sub> and 235 Ar are shown for  $0.5 \cdot k_i^*$  and  $1.5 \cdot k_i^*$ . This exercise makes the case that the uncertainty of the estimated transfer velocities for  $N_2$  and Ar is significantly better than  $\pm 50\%$ , and mostly 237 falls in the range between 5-20%, depending also on the length of the measured time series. 238 The controlled experiment demonstrates the potential of the different gases to trace gas 239 exchange processes. Due to their low solubility and high atmospheric abundance, N<sub>2</sub> and Ar 240 are particularly powerful tracers for gas exchange. The analytical noise in Kr leads to a large 241 uncertainty in deriving the respective transfer velocity. Ar has a signal-to-noise ratio that is 242 only slightly higher than that of  $N_2$ . These differences between gases are fully explained by 243 the abundance and the analytical performance of the applied GE-MIMS method to determine 244

gas concentrations. 16

In summary, we interpret the controlled experiment as a proof of concept of the DGD method.

### $_{248}$ Field Study at La Palme Lagoon

Fig. 3 shows the results of the equilibrium, the observed and the modeled gas concentrations 249 of the La Palme lagoon. The diurnal temperature variation was up to  $10^{\circ}C$ , significantly 250 less than in the tub experiment. For such smaller diurnal temperature amplitudes the exper-251 imental errors of the Kr measurements are too large to estimate the gas transfer velocity in a 252 robust manner. Therefore, in the following only N<sub>2</sub> and Ar results are shown and discussed. 253 The model reproduces the observed data for N<sub>2</sub> remarkably well. Ar concentrations are 254 also reproduced correctly for a large period of the time series. However, in the morning of the second day we observed a decrease in Ar concentrations which are not captured by our simple 256 model. The low concentration may relate to a specific (but unidentified) event or process 257 which affect the Ar but not the N<sub>2</sub> concentration. Such deviation between the measured and 258 the modeled concentration shows how valuable time series of gas measurements over several 259 days are, as they inform on additional processes that affect atmospheric gases in aquatic 260 systems besides atmospheric exchange. However, we have no appropriate explanation for 261 the observed deviation between the measured and predicted Ar concentration. 262

For N<sub>2</sub> two periods with different response dynamics of the in-situ concentrations to the diurnal heating can be observed (indicated with different colors in Fig. 3). For the first period which lasts approximately for the first two and a half days the observed N<sub>2</sub> concentrations are highly damped relative to the atmospheric equilibrium concentrations. For the second period the dampening of the measured to the equilibrium concentrations is much smaller. Further, the phase lag decreases from the first to the second period. Consequently, for the two periods very differing transfer velocities prevail. For the first period:  $k_{N_2}^* = 1.6 \pm 0.2 \, m/d$ . For the second period:  $k_{N_2}^* = 7.1 \pm 0.6 \, m/d$ . Leaving the described discrepancy on the second

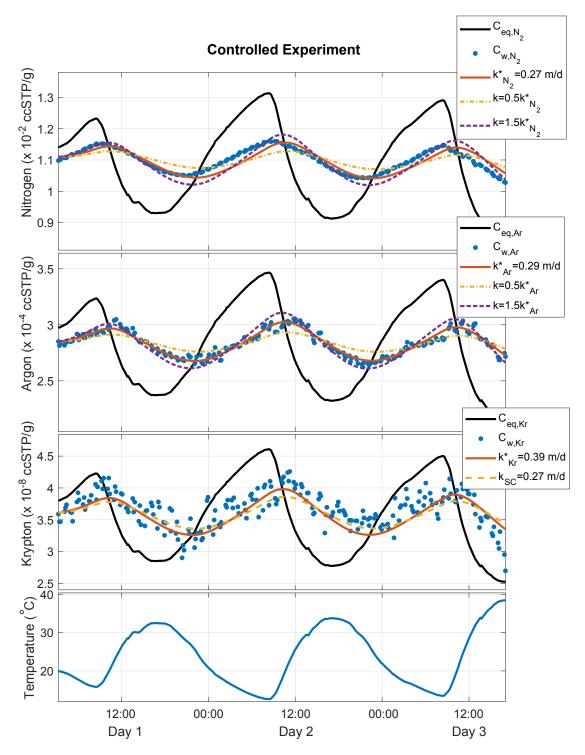


Figure 2: The equilibrium, the observed and the modeled concentrations for  $N_2$ , Ar and Kr (in ccSTP/g) and the water temperature for the controlled experiment and the respective transfer velocities  $(k_i)$ . The model fits the gas concentrations well. The derived gas exchange rates  $k^*$  are:  $k_{N_2}^* = 0.27 \, m/d$ ,  $k_{Ar}^* = 0.29 \, m/d$ ,  $k_{Kr}^* = 0.39 \, m/d$ . To illustrate the sensitivity of the DGD method, transfer velocities 50% larger and smaller than  $k_i^*$  are shown for  $N_2$  and Ar. For Kr the result expected of the transfer velocity scaled from Ar with the Schmidt numbers is additionally shown  $(k_{SC}$  for Kr).

day out for Ar, globally, the same behavior can be found in the Ar time series.

The measurement position within the lagoon is rather sheltered against wind (fetch of approximately  $50 \, m$ ). Thus, during wind-calm conditions waves rapidly dissipate. During the first period wind speeds were low (mean wind speed  $\overline{u}_{10} = 2.9 \, m/s$ ;  $u_{10}$ : measured wind speed scaled to ten meters above the water surface<sup>34</sup>), while during the second period wind speeds more than three times higher were observed ( $\overline{u}_{10} = 10.2 \, m/s$ ). This change was also found in the transfer velocity, and demonstrates the ability of the method to resolve different weather conditions on time scales of hours to days.

### 279 Discussion

The controlled and the La Palme lagoon experiments demonstrate the capability of the DGD method to quantify temporally changing gas exchange rates at specific locations and on relative short time scales. The presented method allows the quantification of the transfer velocity over the wide range of approximately  $0.05-9 \, m/d$  (for  $N_2$ ), which covers the typically observed range of gas transfer for surface waters. The quantifiable range in k/h depends on the magnitude of the diurnal water temperature variation, the temperature dependence of the gas solubility in water and on the measurement precision.

The selection of gases being used as tracers by our method depends on the environmental processes the respective gases are undergoing and on the experimental setup. The noble gases He, Ne, Ar, Kr, Xe and Rn are best suited due to their inert behavior, whereas the gases O<sub>2</sub> and N<sub>2</sub> are subject to biochemical reactions. However, the noble gases He and Rn, in contrast to Ar, Kr and Xe, are released from the sediments by radioactive decay and their concentrations, therefore, depend on e.g. groundwater inflow and circulation of water between surface water and sediments.

From a technical perspective of the noble gases, currently only He, Ar and Kr can be analyzed quasi-continuously, whereas in-situ measurement capability for Ne and Xe using our GE-MIMS instrument remains to be developed. On-going improvements of the experimental

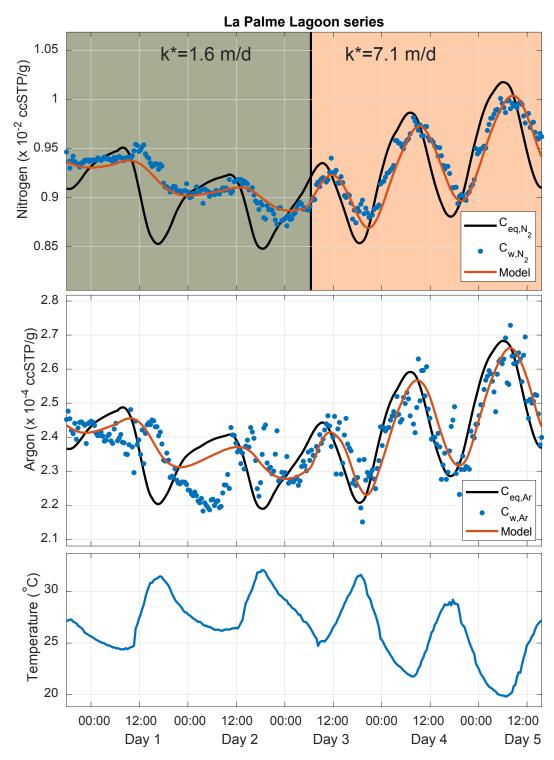


Figure 3: The equilibrium, the observed and the modeled concentrations for  $N_2$  and Ar (in ccSTP/g) and the water temperature series of the water in La Palme Lagoon. The derivation of the transfer velocity for  $N_2$  with the DGD method is split into two periods. The first 2.5 days (green) result in a transfer velocity of  $k_{N_2}^* = 1.6 \pm 0.2 \, m/d$ , while the second 2.5 days (orange) result in  $k_{N_2}^* = 7.1 \pm 0.6 \, m/d$ . Those phases are characterized by very different wind regimes with  $\overline{u}_{10} = 2.9 \, m/s$  for the first and  $\overline{u}_{10} = 10.2 \, m/s$  for the second phase.

performance of (GE)-MIMS systems might increase the number of gases that can be used to analyze air/water partitioning and, thus, greatly expand the determinable range (and the accuracy) of k/h values.

Our experiments show that  $N_2$  and Ar are most sensitive to gas transfer velocities under field conditions given the available technology.  $N_2$  yields the widest k/h range as it has the best signal-to-noise ratio. However,  $N_2$  is potentially non-conservative due to biogeochemical processes, such as denitrification.

The DGD method works best for large daily temperature changes in the water; preferably 304 a water temperature variation of  $10\,^{\circ}C$  prevails to get reliable results and to cover a relevant 305 range of gas transfer velocities. Such high variations are more likely to be found in shallow 306 waters with depths less than a few meters, furthermore, deeper water is unlikely to be 307 vertically well mixed as assumed in our model. Additionally, local conditions can influence 308 the diurnal temperature cycles, including solar radiation, water residence time and heat 309 absorption. These impact the applicability of this method. In rivers, for example, where the 310 method is applicable in principle, 15 this temperature requirement is currently the limiting 311 factor and could be rare to find. Again, improvements in gas measurements expand the 312 locations that can be covered.

The DGD method can be used to quantify temporal variations in transfer velocities, which can then be linked to environmental drivers of air-water exchange, such as wind or river-flow-driven turbulence. For instance, measuring  $k_i$  over a few days with varying wind speeds could be used to derive relationships between transfer velocity and wind speed in shallow environments. It may also be possible to determine the influence of parameters (e.g. precipitation) on near surface turbulence that are less frequently incorporated into the estimation of the gas transfer velocity.

The mass spectrometer used in this study can cycle through multiple inlets on a time scales of minutes, which allows automated analysis at several locations simultaneously. This allows coverage of different geographic conditions at sites, that may be more complex than the open ocean. Hence, site-specific parametrizations can be derived on several orders of areal extents.

As the DGD method does not rely on the application of any artificial tracer, there is no contamination of the environment. With additionally determined quantities e.g. tidal influences, groundwater intrusion or deep water mixing a more complete description of a study site is possible.

Alternative approaches for measuring air-water gas exchange are more labor intensive and
have limited temporal resolution. The DGD method presented here, thus has the potential
to greatly improve on the ability to measure air-water exchange in shallow waters.

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