Spectral artefacts post sputter-etching and how to cope with them – a case study of XPS on nitride-based coatings using monoatomic and cluster ion beams

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Abstract

The issue of artefacts due to sputter-etching has been investigated for a group of AlN-based thin film materials with varying thermodynamical stability. Stability of the materials was controlled by alloying AlN with the group 14 elements Si, Ge or Sn in two different concentrations. The coatings were sputter-etched with monoatomic Ar⁺ with energies between 0.2 and 4.0 keV to study the sensitivity of the materials for sputter damage. The use of Ar_n⁺ clusters to remove an oxidised surface layer was also evaluated for a selected sample. The spectra were compared to pristine spectra obtained after *in-vacuo* sample transfer from the synthesis chamber to the analysis instrument. It was found that the all samples were affected by high energy (4 keV) Ar⁺ ions to varying degrees. The determining factors for the amount of observed damage were found to be the materials' enthalpy of formation, where a threshold value seems to exist at approximately -1.25 eV/atom (~-120 kJ/mol atoms). For each sample, the observed amount of damage was found to have a linear dependence to the energy deposited by the ion beam per volume removed material. Despite the occurrence of sputter-damage in all samples, etching settings that result in almost artefact-free spectral data were found; using either very low energy (i.e. 200 eV) monoatomic ions, or an appropriate combination of ion cluster size and energy. The present study underlines that analysis post sputter-etching must be carried out with an awareness of possible sputter-induced artefacts.

(242 words, 1538 characters)

Keywords

- Sputter artefacts
- Ion-etching
- X-ray photoelectron spectroscopy, XPS
- Gas-cluster ion beams, GCIB
- Coating materials
- Nitrides

Highlights

- XPS analysis performed after different ion-etching methods
- Nitride coatings with different (meta)stability investigated
- Sputter-induced artefacts strongly dependent on material (average) formation enthalpy
- Sputter-induced artefacts linearly dependent on energy deposited per removed volume
- Artefact free spectra can be obtained by both monoatomic and polyatomic ion beams
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1. Introduction

Development of novel materials is a key foundation on which modern technology rests. To be able to understand the structure and the properties of old, and future materials, the use of different analytical techniques to determine the material composition, bonding, structure and morphology is essential. Almost all modern materials analysis techniques are based on irradiating the sample with either particles (electrons, ions, neutrons) or photons (X-rays, UV, visible or infrared light). Additionally, the sample may need preparation before analysis, including irradiating the sample with ions. Such irradiation can have sufficient energy to alter the material - thus post irradiation the surface analysed is no longer the pristine as-received material.

X-ray photoelectron spectroscopy, XPS, is a unique tool for materials analysis. XPS yields information regarding elemental identification of all elements beyond He, quantitative elemental concentrations and information on the chemical environment of each element. Furthermore XPS is a surface sensitive technique with an information depth of three times the attenuation length (AL) of the photoelectrons analysed. For most lab instruments, which commonly use Al K α radiation (hv=1486.7 eV), the AL is a few nm, e.g. for N 1s photoelectrons from AlN is less than 2.5 nm. XPS is an established analytical technique for surface analysis, but there are challenges regarding surface contamination and oxidation.[1]

Since most samples are air-exposed before analysis, they have an oxidised surface layer and adsorbed contaminants. In order to employ surface analytical techniques such as Auger spectroscopy (AES) and XPS to probe the bulk of the material, this surface layer needs to be removed. Such removal is typically performed using an ion source to sputter-etch the surface of the sample. In such sample preparation chemical bonds will be broken. During this process the bulk structure intended for analysis may also be altered. The extent of these changes remains a challenge for sputter cleaning delicate surfaces. The question is how severe are these changes: is the structure and/or chemistry of the analyte changed and if so to what extent? Such modifications may result in changes to the spectral form of the pre and post sputtered materials. For clarity, non-original features will in the following be denoted as artefacts or sputter damage.

Artefacts due to sputter etching have been well known for a long time, and can be divided into two types depending whether the sample composition is changed or not. Changes in the sample

composition occur due to preferential sputtering, where one element is more easily (preferentially) ejected from the sample than other elements. This is often more pronounced in materials where there is a large mass difference between the elements, as well as when the lighter element can form stable gaseous species and thus exit the sample. Preferential sputtering thus typically leads to a change in sample composition as well as a change in chemical environment and/or oxidation state of the remaining elements also giving changes in the spectra of remaining elements. Ceramic materials containing elements that can form gaseous species, and/or contain elements that can have several different oxidation states, e.g. NiO[2], Fe₂O₃[3], WO₃ [4, 5], MoO₃ [5, 6], Ta₂O₅ [7], TiO₂[8], GaN[9], BN[10], are known to be susceptible to preferential sputtering, even if the original material is thermodynamically stable.

However, even if no preferential sputtering occurs, the material can be damaged as bonds are broken and atoms move in the collision cascade that follows the impact of an ion in the keV energy range. This can then lead to the bonding in the material becoming distinctly different compared to prior ion bombardment, thus causing changes to the XPS spectra. Generally organic and polymeric materials, e.g. plexiglass (PMMA) and polyimide [11, 12], and also graphene[13], are known to undergo sputter damage changing the local chemistry upon ion radiation. Also Ar⁺ etching of Si wafer has been shown to affect the valence band in this case due to ion implantation [14]. Reports on artefacts in sulphide [15-17] and carbide [18] based materials as a result of both Ar⁺ sputter etching prior to XPS analysis, and as a result of e⁻ radiation in the TEM analysis [19, 20] are further examples of damage where the local chemical environment is changed, with or without significant preferential sputtering.

Many models as well as simulation schemes of ion-matter interaction have been presented, see e.g. the review by Ignatova et al.[21]. Simpler models often incorporate the mass difference in the irradiated material and surface binding energy to reproduce preferential sputtering, see Malherbe et al. [22]. More complex schemes employ force field models and either Monte Carlo or molecular dynamics simulations [21]. For many compounds it is however difficult to determine surface binding energies, and complex compounds may require specific force field models, limiting the predictive powers of a general model. An alternative initial approach considering the chemical bonding uses the enthalpy of formation [23-27]. For example, Holm and Storp [23] and Christie et al. [24] analysed inorganic salts and found that the free energy of formation was a key parameter for the sensitivity to sputter damage. Such an approach also has the advantage that considering bond energies in compounds also opens up for correlations to other damage than preferential sputtering of one element, such as the decomposition of metastable phases.

From a materials analysis point of view, such as sputter-etching to remove a surface oxide the main question is to what degree data acquired with standard methods can be trusted, and how this can be evaluated. This leads to two new questions: How can one obtain spectra of pristine bulk material and how can artefacts be minimised?

To attain spectra from pristine material, there are in principle two methods. The first option is to ensure that no surface contamination or oxidation occurs prior to analysis. Primarily this is achieved using *in-situ* measurements in ultra-high vacuum (UHV), combining synthesis and analysis equipment, or by ensuring inert transfer from the synthesis equipment to the analysis instrument (for minimal contamination preferably an *in-vacuo* transfer). Such methods have for example been used for the analysis of pure TiN [28] and for electrode materials from batteries after use [29]. Another recently explored method to avoid contamination and oxidation is to deposit a thin capping layer of a light element (e.g., Al), that is thin enough for photoelectrons from the pristine material below to escape during subsequent analysis [30, 31]. Also other techniques such as *in-situ* mechanical polishing[32] and thermal shock induced adhesion failure[33] has been used to gain access to non-oxidised material without using sputter etching. The two latter methods do however require bespoke equipment.

The other option to avoid the need to remove the surface oxide is to increase the information depth of the analysis so that analysis probes below any surface contamination and oxidation. This can achieved by increasing the X-ray energy and therefore the kinetic energy of the photoelectrons [34]. To obtain sufficient information depth hard X-rays with an energy of at least 6 keV are required. This method is known as hard X-ray photoelectron spectroscopy (HAXPES) and thus requires a non-standard X-ray source and an adapted electron analyser. This method is mainly conducted at specialised synchrotron beamlines. There are commercial or semi-commercial X-ray sources with Ag (using the L α line at 2984.4 eV) [35], Cr (using the K α line at 5414.7 eV) [36], and liquid Ga (using the K α line at 9251.7

eV) [37] anodes that give varying degree of HAXPES capabilities to laboratory instruments. However, the X-rays from the Ag source are not energetic enough to be useful for all materials, and the availability of the Cr and Ga sources is very limited. HAXPES has been used both to specifically study sputter-damage as well as to avoid the use of sputter-etching on sensitive materials, see e.g. [15, 18, 38].

If one cannot avoid removing the oxidised surface layer, the obvious way to reduce the amount of damage that may occur upon sputter etching, is to reduce the energy of ions used to bombard the sample. Such an approach has been used with several materials with varying degree of success [9, 10, 18, 39]. Reducing the energy of the ion beam will, however, always lead to a significant reduction in etch rate.

A new approach, which has been gradually developed around the turn of the century, is the use of polyatomic ions for sputter etching. The initial applications used molecular carbon and hydrocarbon ions, primarily C₆₀ bucky balls and C₂₄H₁₂ coronene, which were found to perform well for depthprofiling polymeric materials [11]. However, these carbon-based molecules do not perform well on ceramic materials due to low sputtering yield and unwanted carbide formation. A more recent development is the use of inert gas clusters such as Ar_n⁺ with n up to 5000, which avoids the risk of compound formation due to the use of noble gas atoms [40]. These sources are called gas-cluster ion sources (GCIBS). Cluster formation occurs via supersonic adiabatic isentropic expansion of Ar gas into a vacuum through an aperture. The condensation results in a distribution of cluster sizes. Postionisation mass selection is performed using a mass filter. A more detailed description of the mechanics of cluster formation has been given previously [8, 40]. The clusters are accelerated to a high kinetic energy (several keV) and thus propelled towards the sample. Since the clusters disintegrate upon impact on the sample surface, they transform to a bombardment with many particles of comparably low average energy per particle. For example, an Ar₂₀₀₀⁺ cluster accelerated to a kinetic energy of 15 keV will thus give a bombardment of 2000 Ar atoms, with an average energy of 7.5 eV each. This will lead to a shallow damage zone with very little bulk penetration, and thus less damaged material in the probed analysis volume. However, the impact of the ion cluster also causes non-linear sputtering and implantation effects, which are fundamentally different from impact of monoatomic ions and include a very localised spike in pressure and temperature [40]. The use of Ar_n⁺ clusters have in many cases been shown to successfully reduce, minimise or remove the issue of sputter-damage for a wide range of materials, such as polymers [12], semiconductor materials [41], and oxides [3, 7, 8]. It has also been shown that the cluster size and energy are essential parameters in order to minimise artefacts in the spectra [3, 41].

The present study investigates the issue of artefacts due to sputter-etching for a group of recently studied AlN-based thin film materials from a material analysis point of view. The studied materials are based on pure AlN (a thermodynamically stable phase with strong bonds) and the introduction of a group 14 (formerly known as group IV) elements to form ternary Al-X-N materials, with X being Si, Ge or Sn [42-46]. This series of materials exhibits microstructures with solid solutions beyond the thermodynamic equilibrium and nanocomposite structures, as well as varying average bond strengths. These materials are thus typical examples where material description through force field models is, if not impossible, very challenging and require special expertise (particularly in the case where new materials are synthesised for the first time). From a materials analysis point of view it would hence be convenient if a simpler approach could be used to guide the selection of analysis parameters for new or unknown materials. The present study presents observed correlations between the extent of sputter damage and ion beam parameters and estimations of material stability via the enthalpy of formation. The presented results demonstrate general trends of the studied type materials, but the implications on how to predict sputter damages are relevant also for other materials systems. For this study in-vacuo sample transfer from the synthesis chamber to the analysis instrument was used to obtain reference spectra of pristine material. Sputter-etching with monoatomic Ar⁺ with energies between 0.2 and 4.0 keV were used to study the sensitivity of the materials for sputter damage. The use of Ar_n^+ clusters to remove an oxidised surface layer was evaluated for a selected sample; it was found that (almost) artefact-free spectral data could be attained using this method.

The paper is organised in such a way that background information is introduced for the studied materials and experimental details. The results are divided into three parts, first observations on preferential sputtering made from *ex-situ* experiments, followed by the main study results obtained

from *in-situ* measurement and analysis of photoelectron core levels. This part first considers the core levels that are common for all studies samples (Al 2p and N 1s), followed by the core levels specific for the different materials systems (Si 2p, Ge 2p and 3d, and Sn 3d). From this, quantification of the observed sputter-damage is made, before further observations connected to the valence band spectra are given. The last part of the results are from *ex-situ* experiments where gas cluster ion beams were used to remove the oxidised surface from one of the previously studied samples. This is followed by a section where the results are compared, discussed and put into perspective. Finally the paper is summarised with comments and recommendations for the analyst.

2. Materials

The materials used in the present study have been described in detail in previous publications [42-45, 47], so here only a brief summary is given. The starting point of the sample series is AIN, a thermodynamically stable phase [48]. The series is the created by co-deposition with a group 14 (previously known as group IV) element (Si, Ge or Sn) in various elemental concentrations. These group 14 elements form nitrides, but their stability decreases rapidly downward in the group [48, 49], see Table 1. For tin nitride no data is available, but the reported compound is most likely metastable with respect to the elements. The samples studied here have group 14 element concentration of between 0 and 26 at.%, and have been carefully analysed with XPS, XRD and electron microscopy. Composition and microstructures of the samples in the present study are summarised in Table 2. Using the normalised enthalpy of formation for the binary nitrides (see Table 1) and the sample compositions, a weighted average enthalpy of formation has been estimated for each sample. This calculation assumes the samples are mixtures of stoichiometric binary nitrides, and the estimated values are thus rough approximations.

3. Experimental details

Coatings were synthesised by reactive magnetron sputtering in an AJA 1500C sputter system [42-45, 47]. The base pressure during the depositions was 2.0×10^{-8} mbar or below. For the present study samples were reactively sputter deposited on Si(100) by confocal codeposition from two elemental 2" targets of Al and (Si, Ge or Sn). All depositions were conducted at constant pressure of $4.0-6.0\times10^{-3}$ mbar (depending on the alloying element). Also gas flows were varied depending on alloying element with a relative amount N_2 of 35 to 100%. Higher pressures and higher reactive gas percentage was used for increasing mass of the alloying element. Depositions were conducted at 200 °C, and in the case of Sn as alloying element also with the substrate holder at a -60 V RF bias. The composition was varied by applying different powers to the two magnetrons. For each ternary materials system two samples were deposited with about 10 and 20 at.% alloying element, respectively. Also a binary AlN sample was deposited for comparison. Deposition time was constant at 30 min, resulting in coatings thicknesses between \sim 80 and \sim 270 nm.

Immediately after deposition the samples were transferred *in-vacuo* at pressures below 10^{-9} mbar to the XPS spectrometer using a UHV transfer system described previously [50]. During the subsequent transfer from the storage chamber to the spectrometer the samples were exposed to 2×10^{-8} mbar for <1 min. This procedure ensured that the surface of the samples were not oxidised and that the material could be analysed without sputter-etching.

For comparison, additional samples from the same deposition were removed from the system and thus exposed to air resulting in surface oxidation. One sample was used for *ex-situ* experiments to evaluate if sputter-etching using an Ar_n^+ cluster source could be used to obtain defect-free spectra after removal of the surface oxide.

Both the spectrometers used for XPS (specified below) were calibrated against reference samples of Au, Ag and Cu, according to ISO 15472 [51]. As the samples are electrically insulating, they were measured under constant charge neutralization (specified for respective spectrometer below). In all analyses the Al 2p peak was chosen as charge reference and set to a binding energy of 73.6 eV (which is the literature value for Al 2p in AlN) [52, 53]; all spectra were shifted accordingly. Other alternatives were also considered, but the Al 2p peak position is from a chemical point of view

expected to be least effected to the material, and the approach delivers consistent results as shown by the authors in previous publications [44-46].

For all *in-situ* experiments and for all experiments using monoatomic Ar^+ ion etching XPS was performed using a Physical Electronics Quantum 2000 spectrometer. This instrument employs monochromatic Al K α radiation (hv = 1486.7 eV) and with the used settings provides an energy resolution ~0.65 eV. For the present experiments the analysis spot was set to a diameter of 200 μ m, and an electron take-off angle of 45° was used. Charge neutralization was performed with an electron flood gun and low energy Ar^+ ions, as described in reference [54]. This method will without user input provide stable measurement conditions, but spectra require post measurement charge referencing, specified above. For compositional analysis using data from the Quantum 2000, custom sensitivity factors were derived from reference measurements using a combination of elastic recoil detection analysis (ERDA) and Rutherford backscattering (RBS), details are given in previous publications [44-46].

For the *in-vacuo* transferred samples, spectra were first obtained on the surface of the samples (these spectra henceforth denoted as "pristine"), and after sputter-etching using monoatomic Ar⁺ with three different energies: 200 eV, 1 keV and 4 keV (further details are given in Table 3). The system geometry has an incident angle of Ar⁺ ions of 45° to the sample surface; the ion beam was in all three cases rastered over a 1×1 mm area. Ion beam currents given in Table 3 were measured with a Faraday cup in the system and are typical values for the used settings. The etching time was varied from 35 s to ca. 1 h in order to achieve the same analysis depth of ~30 nm. Sputter-etch rates for the different settings were calibrated using a thin Al-Si-N coating of known thickness. Thus the stated analysis depth will be the same for the different etch settings, but vary slightly between samples due to different composition giving slightly different etch-rates. All four analyses on the samples were performed on four different spots sufficiently separated to ensure no cross-exposure to Ar⁺ ions of other energy than intended, but still within a small enough area (ca 5×10 mm) to ensure no variation in coating composition. Additionally survey spectra and sputter-depth profiles using 200 eV Ar⁺ were obtained for compositional analysis. Bulk compositions were determined from these depth profiles.

Ex-situ experiments to evaluate the use of Ar_n^+ clusters were performed using a Kratos AXIS Supra spectrometer using a monochromatic Al K α source, which has a spectral resolution of 0.44 eV. The instrument uses an electron take-off angle of 90° to the sample surface; this set of experiments was conducted using an analysis spot with a diameter of 110 μ m. The system uses an automated charge neutralizer system [55] to maintain stable measurement conditions for non-conductive samples. Also in this case no user input to the neutralisation is required, but post measurement charge referencing is.

The instrument was equipped with a gas-cluster ion source, which uses post-ionisation mass selection by a Wien filter, allowing for cluster size between n=250 and n=5000. Cluster energy is determined by the accelerating voltage, tuneable between 0.25 kV-20 kV. In the present experiments two ion beam settings were used: one with a large cluster (n=5000) and low kinetic energy (5 keV), and one with a smaller cluster size (n=2000) and a higher kinetic energy (20 keV), see Table 3 for details. In both cases the beam was rastered over an area of 2×2 mm. Sputter-etching was performed, until the oxygen peak was significantly reduced in intensity, to less than 6% and 35% of the original peak area, for the 20 keV Ar $_{1000}^+$ and 5 keV Ar $_{2000}^+$ settings, respectively. Thus the spectra are obtained after most of the surface oxidised layer had been removed. The resulting sputter depths, estimated via rate calibration on a Ta $_2O_5$ thin film standard are also given in Table 3. These depths are smaller than for the monoatomic sputter etching; however the reduction of the oxygen signal shows that they are relevant for the analysis.

Fitting of experimental XPS spectra into their base components was carried out using the XPS Peak software [56]. A Shirley type background was used, and a Voigt profile with a 15% Lorentzian contribution was typically used, although asymmetric contributions were allowed in some cases. Fits were performed simultaneously on several spectra obtained after different Ar⁺ ion bombardments, where the peak shapes were fixed and the intensities were allowed to vary to give an estimate of the different contributions as a function of ion bombardment.

Simulations of the Ar⁺ bombardment of the materials were performed using the SRIM 2013 software package [57] in order to estimate the range of damage and Ar⁺ implantations, and the energy loss depth profiles. This package uses a Monte-Carlo code to simulate the stopping and range of ions in

matter using an amorphous target and a quantum-mechanical treatment of ion-atom collisions [58]. Parameters used for the simulations were kept as close to the experimental conditions as possible, with Ar^+ of different energies hitting an $Al_{0.5}Ge_{0.5}N$ target at a 45° angle, and calculation of full recoil cascades and sputtering. For the simulations 10 000 Ar^+ ions were used. The impact of Ar_n^+ clusters is more complex and cannot easily be simulated in readily available software, and is thus beyond the scope of the present study.

The information depth of photoelectrons can be estimated by considering the photoemission angle, setting the maximum escape length to 3 times the attenuation length of the photoelectrons, of a certain kinetic energy in a certain material. The attenuation length is generally 70-95 % of the inelastic mean free path, which is easier to calculate as is dependent on fewer parameters. As the studied materials are rather complex, and varying composition, the information depth has been estimated for AlN using the inelastic mean free path instead, calculated using the software Quases [59] which employs the TPP-2M equation [60]. This approach will not give an exact value, but is sufficient for the discussion at hand

4. Results

4.1 Ex-situ experiments: preferential sputtering by monoatomic Ar⁺ etching

Sputter-depth profiles using different Ar⁺ ion energies on air-transferred samples revealed that samples in the Al-Ge-N systems suffered from preferential sputtering of N. This is evident from the calculated concentrations (using the same sensitivity factors), which show a decrease of the N content with increasing Ar⁺ ion energies, especially at high alloying contents. For a sample with 28 at.% Ge the measured N content decreased from 52 at.% (using 200 eV Ar⁺) to 40 at.% (using 4 keV Ar⁺). This indicates that N is preferentially removed from the material, and that this occurs to a larger degree, when high ion energies are used for etching. For the combination of high ion energies and high alloying content a significant fraction of N (about 20%) is removed. For the samples Al-Si-N system this effect was very small, in the range of the experimental reproducibility, thus indicating a very low degree of preferential sputtering. For the Al-Sn-N system, depth profiles were (due to limited instrument availability) only obtained using the lowest possible ion energies (200 eV) to minimise the issue. Thus no evaluation of the preferential sputtering can be made for this system. However, considering the relative stabilities of Ge₃N₄ and SnN_x and core level spectra presented below, it is reasonable to assume that the same type of preferential sputtering as in the Al-Ge-N system would be observed in this system as well. All presented compositional data were obtained from profiles using 200 eV Ar⁺ and custom sensitivity factors calibrated against ERDA / RBS measurements. Thus the compositions presented here are correct to within a few atomic percent.

4.2 In-situ sample transfer: analysis of pristine surfaces and effects of monoatomic Ar⁺ etching

Spectra from the measurements conducted after *in-situ* transfer are presented in Fig. 1-4, 6 and 9 The spectra from the pristine surface (green, dotted lines) of the samples show the undamaged material, while the spectra after different etching (blue, orange and red solid lines) exhibit varying degrees of difference compared to the pristine spectra, which are shown in the following to be a consequence of sputter-damage, i.e. artefacts generated by ion etching.

4.2.1. Al 2p and N 1s core level spectra (all samples)

The Al 2p and N 1s spectral regions (Fig. 1-2) show very small differences between the pristine and sputter-etched material for all studied materials. This indicates that the bonding environment of Al and the N in the material does not change. The largest difference in these spectra are a narrowing of the N1s peaks for Al-Ge-N and Al-Sn-N material subjected to high energy Ar⁺ ions. This indicates that the range of chemical environments for nitrogen decreases. A cause of this decrease can be the preferential sputtering of nitrogen in certain chemical environments, i.e. bonded to Ge or Sn. Such an explanation is consistent with the observations of preferential sputtering made above. The observed variations of the Al 2p and N 1s spectra for the binary AlN sample, (possibly also the Al-Si-N samples) give an indication of the uncertainties of the used experimental set-up and charge-referencing method. The core-level spectra of the alloying elements are described below and presented in Fig. 3 – 5. Each materials system will be presented independently, and trends discussed later.

4.2.2. Al-Si-N – Si 2p core level spectra

For the Si 2p region (Fig. 3) two different artefacts are noted: firstly, there is a small, although systematic shift of the peak to lower binding energy (101.4 – 101.1 eV and 101.2 – 100.9 eV, for low and high alloying content, respectively) as the material is subjected to higher energetic ion bombardment. Secondly, there is a formation of a low binding energy shoulder. This shoulder is centred at 98.7-99.3 eV, and is thus consistent with Si in the elemental state [61]. The second feature is more prominent for the spectra attained after sputter-etching with higher ion energies. The changes, compared to the pristine surface (green dashed spectra), are minor and almost non-existent in the spectra attained after etching with 200 eV Ar⁺.

4.2.3. Al-Ge-N – Ge 2p and 3d core level spectra

In contrast to the Al-Si-N system, the analogous Al-Ge-N system with its lower thermodynamic stability, exhibits large changes for the material subjected to high energy Ar^+ bombardment, as evidenced by the Ge core level spectra (Fig. 4). The pristine peak at higher binding energy (1219.2 eV and 31.4 eV for Ge $2p_{3/2}$ and Ge 3d peaks, respectively, typical for Ge bonded to N) gradually decreases in intensity at higher sputter energies, while a low binding energy feature increases and gradually shifts to a position in agreement with elemental Ge (1217.0 eV and 29.2 eV, respectively). For the highest alloying content and ion energies (4 keV) the Ge in the material appears completely reduced to the metallic state.

It is worthwhile noting that Ge provides two core level lines within the range accessible for Al K α excitation: the 3d-line at a binding energy of ca 30 eV, and the 2p lines at ca 1218 eV. The photoelectrons have different kinetic energy and therefore different escape depths, ~18 Å for Ge 2p and ~63 Å for Ge 3d photoelectrons [59, 60]. This gives rise to a distinct difference observed in the top and bottom spectra shown in Fig. 4 a and b: Namely that the Ge 3d spectra, originating from larger depth, show less damage. This is especially clear for the spectra obtained after etching with 1 keV Ar $^+$. These observations can be understood by considering the depth at which the impinging Ar $^+$ ions lose their energy, which were simulated using the SRIM 2013 software. Fig. 5 shows the calculated energy loss of Ar $^+$ ions of different energy as a function of depth. As can be seen, the 200 eV Ar $^+$ lose practically all their energy (90%) within 10 Å, and the 1 keV and 4 keV ions lose their energy within 22 Å and 53 Å, respectively. It is thus clear that in the case of low energy Ar $^+$ bombardment the photoelectrons from the 3d orbitals to a large extent originate from pristine material, below the damaged region, thus explaining the appearance of two rather distinct contributions of different intensity for Ge 2p and Ge 3d spectral regions.

4.2.4. Al-Sn-N – Sn 3d core level spectra

For the Al-Sn-N material the alloying element (i.e. Sn) core levels exhibit large changes when subjected to Ar⁺ ion bombardment, see Fig. 6. As for the Al-Ge-N coatings, the observed damage consists of a gradual metallisation of the Sn core level as the energy of the Ar⁺ is increased: the Sn 3d_{5/2} peak transforms from a symmetrical peak at 486.3 eV (consistent with Sn in a nitride environment) to an asymmetrical peak at 484.2 eV (consistent with metallic Sn). Considering that the other observed peaks from the same sample (Al 2p, N 1s and valence band, see Fig. 1, Fig. 2 and Fig. 9) are not shifting, the observed shift for Sn 3d must be due to a change in chemical environment, not charging. The sample with higher alloying content is more affected by the bombardment, and almost no contribution from tin nitride is visible after 4 keV Ar⁺. However, for both high and low Sn concentrations the fraction of reduced Sn (artefacts as defined in the following section 4.2.5) in the spectra obtained after sputter-etching with 200 eV Ar⁺ is limited.

4.2.5. Quantification of sputter damage

For the core level spectra (Si 2p, Sn 3d and Ge 3d) considered above, the extent of sputter-damage can be estimated via peak fitting. An example using the Sn 3d spectrum from the low Sn-content sample after sputter-etching with 1 keV Ar⁺ is shown in Fig. 7. Peak fitting was performed by using two peaks: one with fixed position, shape and width according to the pristine spectra; and one peak with fixed shape and width according to a best-possible fit to the most damaged sample. Fits were made on the spectra obtained after ion bombardment of varying energies by changing the intensity of these two contributions and also letting the position of the damage-peak vary. As evidenced by the difference spectrum (experimental - peak sum) in Fig. 7, this simple procedure does not give a perfect fit, but is sufficient to make an estimate of the extent of artefact formation. In the case shown, 60% of the signal originates from sputter-induced artefacts. A more detailed analysis would include more contributions

and give better fits. This would perhaps also give additional information on the nature of the damaged material, but as this would include substantial uncertainties and is not the focus of the present study. Thus, the simpler approach which is sufficient to discuss trends in sputter damage is used.

Similar fits were conducted for all ternary samples (in the case of Al-Si-N, also the pristine peaks were allowed to shift by a small amount). The results of curve fittings are presented in Fig. 8, where the relative amount of artefact signal is plotted against Ar⁺ ion energy, and **Error! Reference source not found.** Table 4 where additional details are provided. There are clear trends with respect to ion energy, alloying element and alloying concentration: The amount of sputter-damage increases with increased ion energy and alloying concentration, and also downward in group 14. The latter clearly correlates with the bond strength A-N (A=Si, Ge, Sn), as well as increasing mass difference in the samples. The information depth of the peaks used in damage evaluation are similar, varying between 4.7 nm (Sn 3d) and 6.3 nm (Ge 3p), and thus allow for a valid comparison.

4.2.6. Valence band spectra

The valence band spectra reflect the chemical bonding of a material, since the energy of chemical bonds are of the magnitude of the observed binding energy range, i.e. 0 to 20 eV. Clear changes are observed for all samples after different ion bombardments, as shown in Fig. 9. In contrast to the core level spectra described above, the valence band spectra of all samples in the present study are affected by Ar⁺ ion etching, including the single phase AlN sample.

In agreement with core level spectra, the changes increases with ion energy and with increased alloying content. Two additional peaks appear at 23.0 and/or 9.2 eV post ion bombardment. These can be attributed photoelectron peaks from Ar 3s and 3p, respectively [14, 62], thus showing Ar implantation. This is also confirmed by survey spectra taken after sputter-etching with 4 keV Ar⁺ (not shown), which all show Ar 2p peaks which were not present on the pristine surface.

Furthermore, there is also a clear tendency of increased intensity at the Fermi level. This is most notable for high-alloying content Al-Ge-N and Al-Sn-N samples and reflects the metallisation of the alloying element, as described above. This appearance of metallic states at the Fermi edge goes in parallel with the decrease of the bonding N 2p-metal 3d hybrid state at ca. 6 eV for Al-Ge-N and ca. 5 eV for Al-Sn-N [44, 63]. Similar, although smaller artefacts are visible also for the Al-Si-N as well as the AlN samples at higher Ar⁺ energies.

4.3 Ex-situ experiments: removal of surface oxides with Ar_n⁺ cluster ions

A recently developed technique to sputter clean surfaces with minimal sample damage is the gas cluster ion source (GCIS) [40]. In order to compare this new technique to traditional argon ion sputtering, one sample from the same deposition as a previously investigated sample was selected. The selected sample was the Al-Sn-N-sample with high alloying content, i.e. the most sputter-sensitive sample in the present study, which had been exposed to atmosphere before analysis. This sample was analysed after removal of the surface oxide using an Ar_n⁺ cluster ion source. As shown in Table 3, two settings were used: a smaller cluster with high energy (Ar₁₀₀₀⁺, 20 keV), and a larger cluster with low energy (Ar₂₀₀₀⁺, 5 keV). The obtained spectra are shown in Fig. 10 (solid lines) together with reference data from the *in-situ* experiments described above (dotted line). The spectra after etching with 5 keV Ar_{2000}^{+} (blue curves in Fig. 10) are almost identical to the reference spectra. In contrast to the spectra recorded after etching with 200 eV monoatomic Ar⁺, there is no visible low-energy shoulder in the Sn 3d peak. There is although a small shift of the Sn 3d peak to higher binding energies, which most likely is connected to that not all surface oxide has been removed (as stated above the oxygen signal was reduced to 35% by this sputter-etching). Also the valence band spectrum in the binding energy region up to 15 eV is unaltered, compared to the *in-situ* reference. This shows that artefact-free spectra of the bulk can be obtained using Ar_n^+ cluster etching. However, the spectra recorded after etching with 20 keV Ar₁₀₀₀⁺ (red curves in Fig. 10) are distinctly different from the *in-situ* reference spectra, and show large similarities to that observed for monoatomic Ar⁺ ion beam with an energy of 4 keV. This shows that using Argon clusters and working with inappropriate settings (in this case. Ar_{1000}^+ , 20 keV) may cause damages as severe as monoatomic sources. It must although be noted that the tested sample is extremely sensitive to energetic ion radiation, and is thus an extreme test.

5. Discussion

5.1 Observed damage by monoatomic etching

The presented results using traditional monoatomic ions are in good agreement with literature (e.g. [18]), confirming that low energy monoatomic ions used for sputter-etching significantly decrease the amount of sample damage. Fig. 8 is remarkably similar to the data presented in reference [18], indicating a common mechanism for the observed damage. It is also important to note that for very low energy Ar⁺ (200 eV) the obtained spectra for even the most sputter-sensitive Al-Sn-N are almost artefact-free, and can thus be used for the analysis of *ex-situ* transferred material. Such measurements have also been performed by the authors, and presented in the publications focused on respective materials, see references [44-46]. No additional features were observed as an effect of using the sputter-etching to remove the surface oxide.

There are two principle reasons why the spectra obtained post monoatomic 200 eV Ar⁺ bombardment show less damage. The first is connected to the depth to which the energy of the Ar⁺ ions is deposited, in comparison to the information depth of the observed photoelectrons, i.e. to what extent the pristine material can be analysed. The second relates to the amount of energy deposited in the material during ion bombardment, i.e. the amount of energy which can cause damage.

The first of these two points is illustrated by the results in Fig. 4 where the different information depths of the Ge 3d and 2p core levels (18 and 63 Å, respectively) and different penetration depths of the Ar⁺ ions are presented. At lower ion beam energy the damaged zone is shallower, and at sufficiently low ion energies the information depth of the probed core levels (Si 2p, Ge 3d and Sn 3d) will be large enough that the recorded signal will be mainly obtained from the pristine material below the damaged surface, hence significant pristine signal after etching with 200 eV Ar⁺ ions.

The second point is illustrated by considering how much energy is deposited by the impinging ions. As previously illustrated in Fig. 5, the energy of each Ar⁺ ion will be deposited within a certain depth. Normalizing the kinetic energy of each ion by this penetration depth will give a measure of how much energy is deposited per unit depth in the material. In Fig. 11a, the relative amount of sputter damage is plotted *vs* the ion energy (E) per penetration depth (D), where D is taken from Table 3. The fraction of sputter damage rises close to linearity with E/D, with different gradients for the different samples. The slope of these linear relations is a measure of the sputter sensitivity (the information depth of the observed core levels are roughly the same: 47-63 Å, and thus comparable). This illustrates that, despite the larger penetration depth of more energetic ions, the sputter damage scales directly with the depthnormalised energy of the Ar⁺ ions; and explains why less damage is observed after using 200 eV ions.

An alternative, macroscopic way of estimating the relative amount of deposited energy is to consider the total dose of ions (given by the beam current and sputtering time) and the volume of removed material (from sputter depth and ion beam raster area). This results in a measure of energy per volume $(eV/Å^3)$, see Table 3. If the fraction of sputter damage is plotted against this parameter, an almost identical plot to Fig. 11a is obtained (see Fig. 11b). Since sputter depth as well as area was kept constant the parameter of importance is the total dose of ions, which mainly depends on the sputter rate of each setting (itself a function of ion energy and current). Thus, despite a distinctly larger dose of ions for the lower kinetic energy settings, the amount of energy deposited per removed volume is greater for the higher kinetic energy settings, and scales directly to the amount of observed artefacts in the material.

5.2 Comparison of etching by GCIB to monoatomic Ar⁺

For researchers interested in the surface analysis of sputter-sensitive materials, the results presented in this investigation illustrate three important points connected with the use of GCIS:

a) The use of an Argon ion cluster source for etching can successfully be employed to obtain almost artefact-free spectra, also for sensitive inorganic materials. However, as clearly shown by the differences between the spectra in Fig. 10, the use of an ion cluster beam is no guarantee for artefact-free spectra. Using the appropriate cluster size and cluster energy is essential when analysing sputter-sensitive materials. Two extremes settings for the GCIS were investigated here, namely maximum and minimum energy per Ar atom. In-between there is a wide field of useful settings, illustrating the need for further studies to understand, which parameters are decisive for the observed material damage.

- b) In the case for the minimum setting used here, the average energy per atom for the 5 keV $\operatorname{Ar}_{2000}^+$ amounts to 2.5 eV (see Table 3), which is in the same order of magnitude as the formation enthalpy for the investigated nitrides (see Table 1 and Table 2). An increase to the maximum setting of 20 kV $\operatorname{Ar}_{1000}^+$ (20 eV/atom) causes damage to the very sputter-sensitive Al-Sn-N sample, despite the fact that almost artefact-free spectra are attained after etching with monoatomic 200 eV Ar^+ . This demonstrates that average energy per particle is not the solely determining parameter for sputter damage. The dose is seemingly also of importance, but also the impact collision mechanics of the Ar_n^+ gas cluster should be considered, and as pointed out by Simpson et al.[7] the thermal spike that occurs upon impact [40] may play an important role in causing damage.
- c) It must be stated that for performing conventional depth profiling experiments for inorganic materials with a layer thicknesses greater than 10 nm it is impractical to use cluster ion beam acceleration energies of less than 10kV due to the low sputter etch rate. The low energy cluster mode (5 keV Ar₂₀₀₀⁺ kV) is suitable for sputter cleaning thin oxide films, not so for thicker materials.

5.3 Sputter sensitivity and thermodynamic stability

Also from a materials point of view a few trends are worth noting. One is that sample damage occurs also on thermodynamically highly stable systems such as single phase AIN, see e.g. top spectra in Fig. 9, where 1 and 4 keV Ar⁺ cause small changes to the valence band. However, it is clear that this sample is least affected in the present study. From Fig. 8 it is clear that the amount of damage sustained by the samples is correlated to the concentration of the alloying element. This can be illustrated by plotting the relative amount of sputter damage in the XPS core level spectra as a function of the weighted average of the standard enthalpy of formation (see Table 2) for the respective sample, as shown in Fig. 12. For the samples in the present study the trends are clear: The enthalpy of formation of the material determines whether sputter damage occurs and the ion energy largely determines to what degree sputter damage occurs. The spread of the data points is large, probably due to the rough estimation of the formation enthalpy and possibly due to errors in estimating the amount of damage (c.f. Fig. 7 and section 4.2.5). The threshold for substantial damage seems to be at a formation enthalpy of -1.25 V/atom (~ -120 kJ/mol atoms).

Similar trends as those observed in the present work have been seen previously; the early studies of Christie et al. [24] demonstrated that for group 2 and 14 metal carbonates, sulphates and nitrates the observed damage due to a monoatomic Ar⁺ ion beam could be directly correlated to the free energies of formation: significant damage (using a 3 keV Ar⁺ beam) occurred for salts with formation enthalpies between 0.5 and 1.6 eV/atom (50-153 kJ/mol atoms), however salts with formations energies of ca 2.5 eV/atom (240 kJ/mol atoms) sustain much less damage.

Since the cluster ion experiments were only conducted on a single sample, the above discussed trends cannot be confirmed for gas cluster ion sputtering using the present data. However, Barlow et al. [41] investigated a number of binary semiconductor compounds using sputter-etching with an Ar_{1000}^+ source, and found that one compound (InAs) was much more sensitive to damage than the other compounds (CdTe, GaAs, GaP, ZnSe and Hf O₂). The damage could (as here) be avoided by lowering the energy of cluster beam, from 6 to 2 keV. Not explicitly considered by Barlow et al. was the standard energy of formation for the studied compounds. It is although interesting to note that InAs has the lowest $\Delta_f H^\circ$ of the studied compounds with -58 kJ/mol (\sim -0.6 eV/formula unit), with the other compounds ranging from -71 kJ/mol (GaAs) to -1145 kJ/mol (HfO₂) [48]. This thus fits with the trends observed in the present study with a threshold value for damage to occur (as the difference in formation energy between InAs and GaAs is small), but with a lower threshold value (\sim 0.35 eV/atom) which is consistent with the differences in damage mechanisms for monoatomic and cluster ion sputter-etching.

For the present studied AlN-based solid solutions and nanocomposites, the stability is strongly dependent on the weaker nitride bond, and the observed damage is reduction of the weaker nitrideforming element (i.e. Si, Ge and Sn). This suggests that the damage that occurs is preferential sputtering of the N atoms bonded to the weaker nitride forming metal (or semi-metal), leading to a reduction of this element. This is supported by the position and shape of the damage peaks in the core levels (see Fig. 1 through 4 and 6.), the increase of intensity at the Fermi level (see valence band

spectra in Fig. 9), as well as the narrowing of the N1s peak, and the depletion of nitrogen in the samples upon sputter etching.

5.4 Limits to acquisition of artefact-free surface information

Without knowing *a priori* the sputter sensitivity of a material it is not possible to know the extent of artefact formation after a sputter cleaning. By comparing spectra obtained after exposure to different sputter conditions one can obtain information on the form of artefacts produced. The only way of knowing if spectra are artefact-free, is the comparison to an unexposed reference samples.

In the present work *in-vacuo* transfer was conducted to obtain reference spectra. Such a procedure requires customised equipment (vacuum transfer system and adapted deposition and XPS systems). Despite such efforts, the pristine surface may not be representative of the bulk of the material, as during growth many materials exhibit varying degrees of surface segregation, which means that e.g. one element may be over-represented in the surface near region. Also the approach using a capping layer to protect the surface suffers from the same issue, but it also puts extreme demands on the capping layer – it must be dense enough to hinder oxygen to reach the material underneath, and at the same time thin enough to be electron transparent for the photoelectrons that are analysed.

HAXPES has been used to obtain reference spectra without sputter cleaning, e.g. [15, 18]. This method also requires specialised equipment (a customized XPS system, or a dedicated beamline at a synchrotron facility) and also has the inherent problem that spectra will always contain information from the surface. Difference spectra between surface sensitive and more depth sensitive spectra is a way to counteract this, but such a procedure also adds to the general uncertainties, and the possibility that the near-surface region is not representative of the bulk is still an issue. To be aware of these issues connected to the reference methods is important in order not to over-interpret results in one direction or the other.

6. Summarising remarks

The present study demonstrates that sputter artefacts are an unwanted reality and need to be considered when using sputter-etching to gain access to the bulk of a material e.g. via performing sputter depth profiling to analyse different layers. It has also been demonstrated that an Ar gas cluster ion source can be used to obtain artefact-free spectra after etching, even for highly sensitive (inorganic) materials. However, using appropriate cluster energy and size is essential to obtain such results. To a large extent artefacts can also be avoided using very low energy (i.e. 200 eV) monoatomic ion beams, but at the cost of etching speed. In any case analysis must be carried out with an awareness of the possible artefacts which can be created. It has been shown for the case of AlN that also the chemical states of single-phase, thermodynamically stable materials can be affected of high energy (4 keV) ions. Furthermore it has been shown that the enthalpy of formation of the studied materials is the determining factor for the materials sensitivity to sputter-damage. For monoatomic Ar⁺ etching of AlN-based materials a threshold value seems to be present at about -1.25 eV/atom (~ -120 kJ/mol atoms). A comparison to literature although makes it plausible that similar values are applicable also to further material systems.

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Tables

Table 1 Thermodynamic data for the group 14 nitrides. $\Delta_f H^{\circ}$ is the standard enthalpy of formation [48, 49]. In the second and third data columns normalisation has been done with respect to number of atoms in the respective compound.

Compound	$\Delta_{\rm f} { m H}^\circ$ (kJ/mol compound)	normalised $\Delta_f H^\circ$ (kJ/mol atoms)	$\begin{array}{c} \text{normalised } \Delta_f H^\circ \\ \text{(eV/ atom)} \end{array}$		
AlN	-318	-159	-1.65		
Si_3N_4	-851	-122	-1.26		
Ge_3N_4	-63	-9	-0.09		
SnN_x	n/a	n/a	n/a		

Table 2 Summary of samples investigated in the present study. Compositions from XPS measurements, phase content from XRD and TEM, thickness from SEM. The average Δ_tH° is is estimated from the standard energy of formation of the binary nitrides (see Table 1) and the elemental composition of respective sample.

Sample	Composition (at.%)				Microstructure	Phase(s)	Coating thickness	Average $\Delta_{ m f}{ m H}^{\circ}$
•	Al Si/Ge/Sn N O		•		(nm)	(eV/ atom)		
AlN	46	0	54	< 1	single phase	AlN	~80	-1.65
Al-Si-N low [Si]	34	11	55	< 0.5	nanocomposite	$nc-(Al_{1-x}Si_x)N/a-Si_3N_4$	~110	-1.44
Al-Si-N high [Si]	25	20	55	< 0.5	nanocomposite	$nc-(Al_{1-x}Si_x)N / a-Si_3N_4$	~140	-1.36
Al-Ge-N low [Ge]	32	12	56	< 0.5	single phase	$nc-(Al_{1-x}Ge_x)N_y$	~170	-0.75
Al-Ge-N high [Ge]	22	26	52	< 0.5	nanocomposite	nc - $(Al_{1-x}Ge_x)N_y / a$ - GeN_z	~270	-0.38
Al-Sn-N low [Sn]	36	10	54	< 0.5	single phase	$nc-(Al_{1-x}Sn_x)N_y$	~130	-0.84
Al-Sn-N high [Sn]	28	21	51	< 0.5	single phase	$nc-(Al_{1-x}Sn_x)N_y$	~220	-0.45

Table 3 Sputter-etching parameters used in the study with monoatomic Ar^+ conducted with a Physical electronics Quantum 2000. Etching with polyatomic Ar_n^+ -clusters conducted in a Kratos AXIS Supra spectrometer. Values of ion current are typical for respective instrument settings. Both relative dose and deposited energy is given per removed volume of material, thus compensating for both different sputter depth and area. D is the depth at which 90% of the energy of monoatomic species has been deposited according to SRIM simulations (c.f Fig. 8). Sputter rates for argon cluster experiments are calibrated to Ta_2O_5 thin film standard

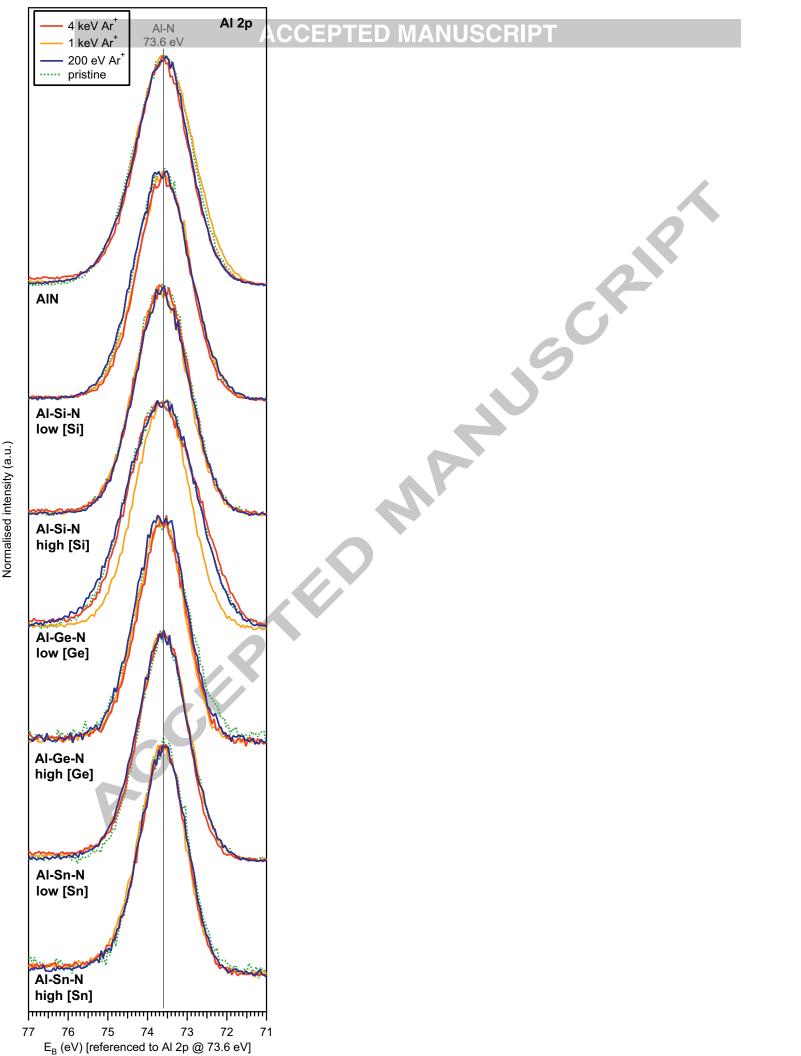
Setting	Ion used	Energy / atom or ion (eV)	Ion current (µA)	Sputter time (s)	Sputter depth (nm)	Etch rate (nm/min)	Relative dose (atoms/nm³)	Deposited energy (eV/ų)	D (nm)
Ar 200 V	Ar ⁺	200	0.115	3460	30	0.5	83	17	1.0
Ar1 kV	Ar^+	1000	0.312	690	30	2.6	45	45	2.2
Ar 4 kV	Ar ⁺	4000	2.700	35	30	51	20	79	5.3
Ar ₂₀₀₀ 5 kV	Ar_{2000}^{+}	2.5	0.045	600	<5*	<0.5*	n/a	n/a	-
Ar_{1000} 20 kV	Ar_{1000}^{+}	20	0.020	45	12*	16*	117	2	-

Table 4 Results of peak fittings for evaluation of relative amount of sputter-etching artefacts. For each fitted component E_B specifies the peak position, fwhm the full width at half maximum, %L the Lorentzian contribution to the Voigt function, and asymmetry gives the tail strength and length parameters. Amount of artefacts refer to the relative intensity of the damage component compared to the entire peak intensity. The latter is also plotted in Fig. 8. An example of the peak fittings are shown in Fig. 7.

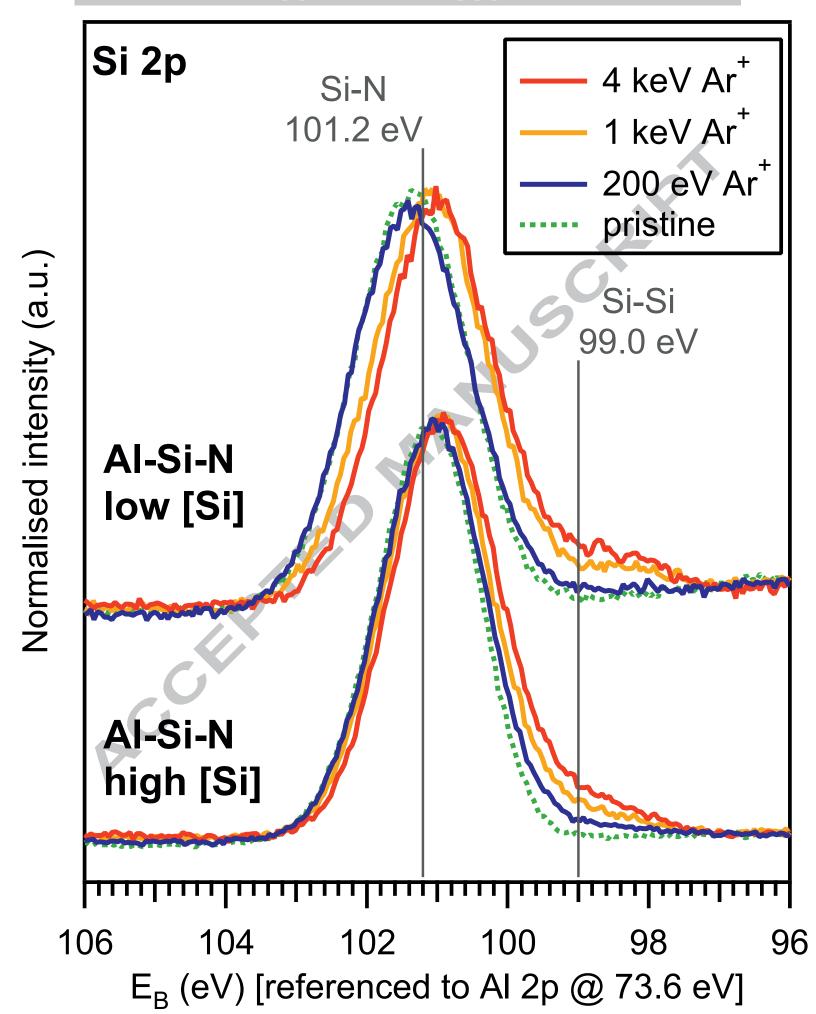
	Peak	Pristine component			Damage component				Amount of artefacts (%)		
Sample		E _B (eV)	fwhm (eV)	% L	E _B (eV)	fwhm (eV)	% L	asymmetry	200 eV	1 keV	4 keV
Al-Si-N low [Si]	Si 2p	101.4-101.1	1.9	0	98.7	1.6	20	n/a	0	5	8
Al-Si-N high [Si]		101.2-100.9	1.7	0	99.3	2.2	20	n/a	4	8	14
Al-Ge-N low [Ge]	Ge 3d	31.4	2.1	15	28.9-29.2	2.0	7	0.8 / 15	14	39	69
Al-Ge-N high [Ge]		31.4	1.7	15	29.6-29.2	1.5	7	0.8 / 15	19	60	82
Al-Sn-N low [Sn]	Sn 3d5/2	486.2	1.6	15	484.9-484.7	1.4	30	0.3 / 50	26	60	85
Al-Sn-N high [Sn]		486.3	1.5	15	485.1-484.6	1.2	30	0.3 / 50	27	71	95

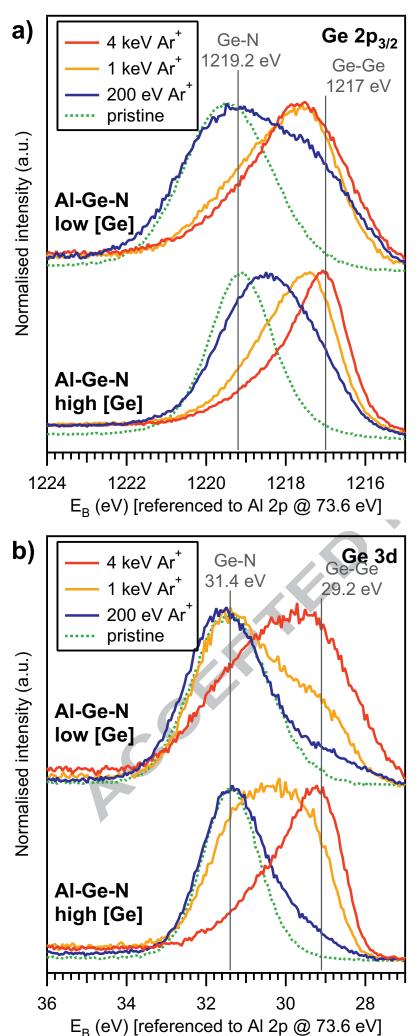
Figure captions

Fig. 1 XPS spectra of the Al2p region from in-situ experiments of all samples. The four spectra per sample show spectra attained on the surface (green, dotted line), and after sputter-etching using 200 eV (blue solid line), 1 keV (yellow solid line) and 4 keV (red solid line) Ar⁺ to a depth of ca 30 nm. (Colour online) XPS spectra of the N1s region from in-situ experiments of all samples. The four spectra per sample show spectra attained on the Fig. 2 surface (green, dotted line), and after sputter-etching using 200 eV (blue solid line), 1 keV (yellow solid line) and 4 keV (red solid line) Ar⁺ to a depth of ca 30 nm. (Colour online) Fig. 3 XPS spectra of the Si2p region, from in-situ experiments. The four spectra per sample show spectra attained on the surface (green, dotted line), and after sputter-etching using 200 eV (blue solid line), 1 keV (yellow solid line) and 4 keV (red solid line) Ar⁺ to a depth of ca 30 nm. (Colour online) XPS spectra of the Ge 2p_{3/2} (a) and Ge 3d (b) regions, respectively, from in-situ experiments. The four spectra per sample show Fig. 4 spectra attained on the surface (green, dotted line), and after sputter-etching using 200 eV (blue solid line), 1 keV (yellow solid line) and 4 keV (red solid line) Ar⁺ to a depth of ca30 nm. (Colour online) Fig. 5 Energy lost by impinging Ar+ ions as a function of depth in the material, estimated by SRIM simulations. Different ion energies shown in colour: 200 eV (blue), 1 keV (yellow) and 4 keV (red). Solid lines show loss at depth (left axis), and dashed lines show cumulative loss (right axis). Solid vertical lines mark the information depth (ID) of the Ge 2p and Ge 3p spectral regions. (Colour online) Fig. 6 XPS spectra of the Sn3d region from in-situ experiments. The four spectra per sample show spectra attained on the surface (green, dotted line), and after sputter-etching using 200 eV (blue solid line), 1 keV (yellow solid line) and 4 keV (red solid line) Ar to a depth of ca 30 nm. (Colour online) Peak-fitting of the Ge 3d_{5/2} peak to estimate amount of sputter-damage artefacts. The sample is a low-alloying content AlSnN; the Fig. 7 spectrum was recorded after sputter-etching to a depth of 30 nm using 1 keV Ar⁺ (c.f. Fig. 6 top, yellow curve). Estimated amount of sputter-damage for all samples in the present study as a function of Ar+ energy. The amount of sputter-Fig. 8 damage is estimated by peak-fitting (c.f. Fig. 7) of the Si 2p, Ge 3d and Sn 3d5/2 peak respectively. The information depth of these photoelectrons is between 5 and 6 nm. Fig. 9 XPS spectra of the valence region from in-situ experiments of all samples. The four spectra per sample show spectra attained on the surface (green, dotted line), and after sputter-etching using 200 eV (blue solid line), 1 keV (yellow solid line) and 4 keV (red solid line) Ar⁺ to a depth of ca 30 nm. (Colour online) XPS spectra from ex-situ measurements of the high alloying content Al-Sn-N sample after removal of surface oxide with Ar_n⁺ Fig. 10 cluster ions (solid lines). Reference spectra from in-situ experiments in another system are shown for comparison (dashed line). (Colour online) Fig. 11 Estimated amount of sputter-damage for all samples in the present study as a function of ion energy per depth (a) or removed volume of material (b) The amount of sputter-damage is estimated by peak-fitting (c.f. Fig. 7) of the Si 2p, Ge 3d and Sn 3d5/2 peak respectively. The information depth of these photoelectrons is between 5 and 6 nm. Correlation between amount of sputter damage sustained by the samples, and the estimated standard enthalpy of formation for the Fig. 12 ternary samples, see Table 2. Dashed lines are only intended as guides for the eye.

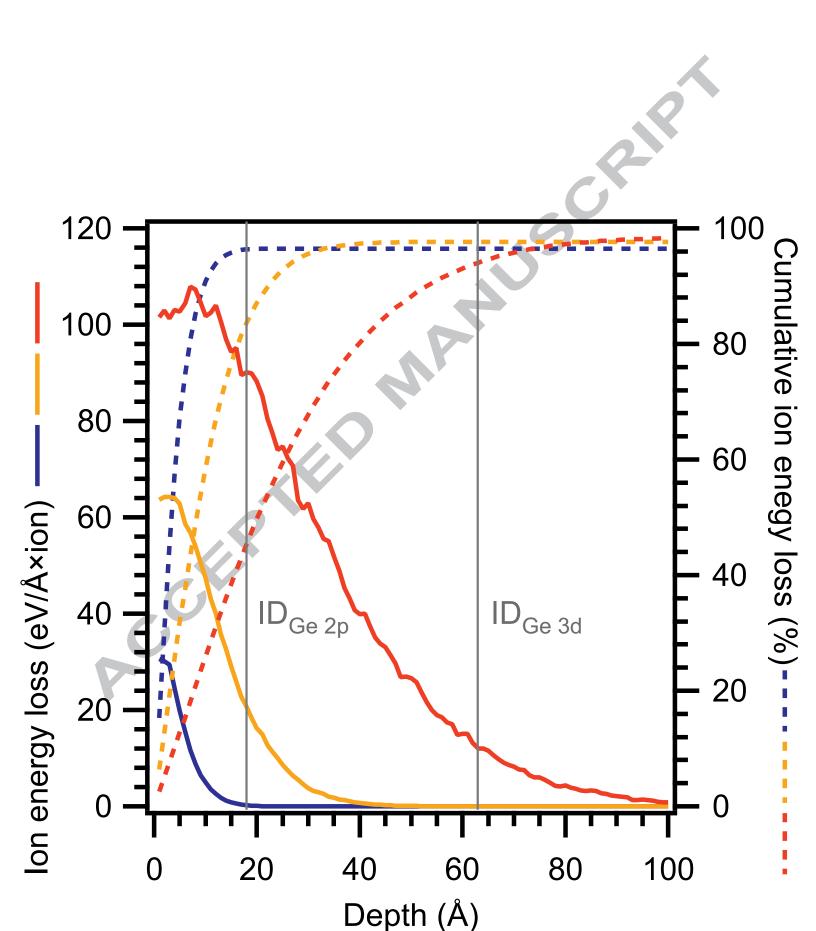


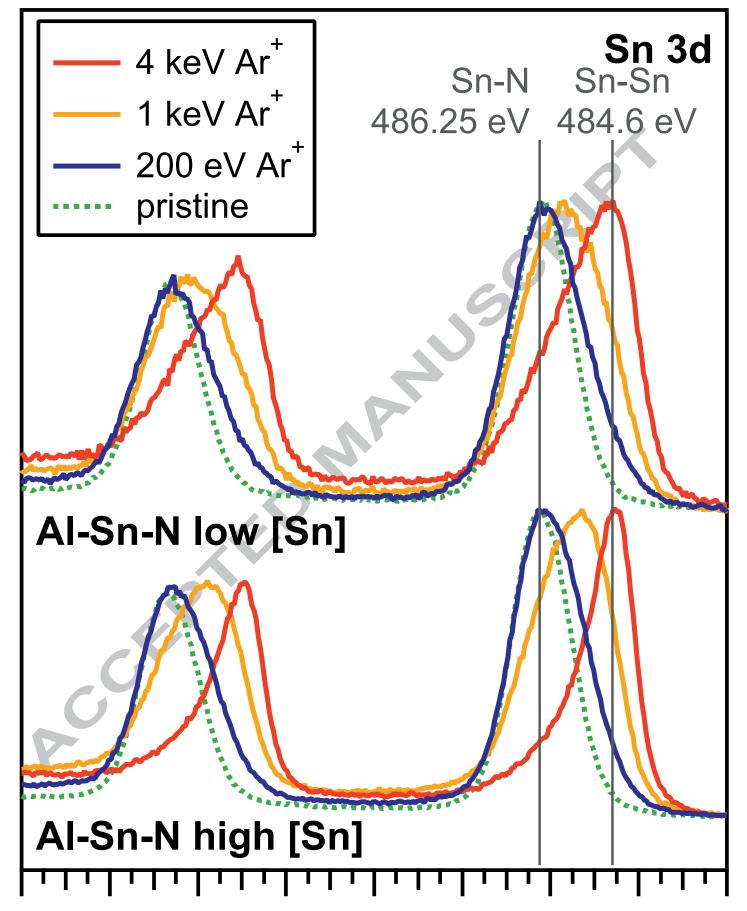
Normalised intensity (a.u.)



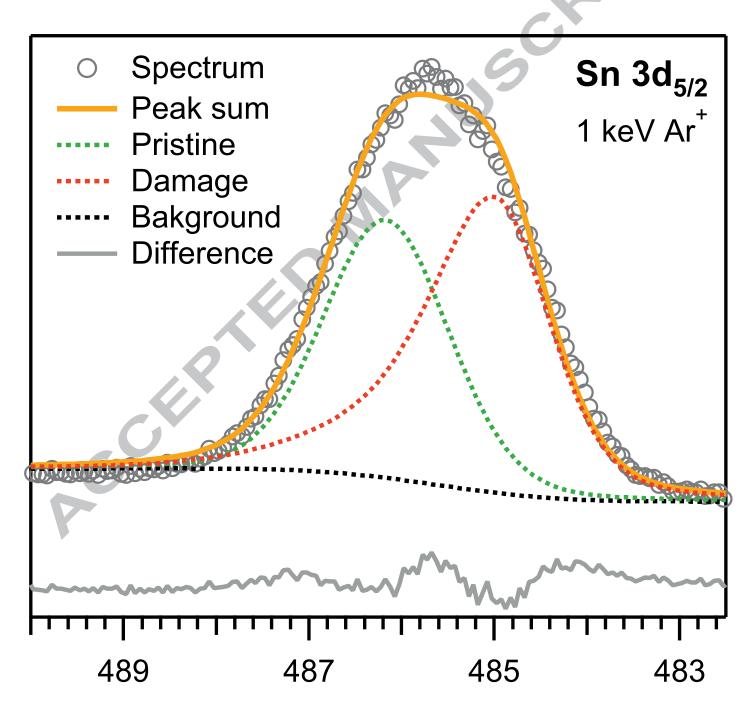


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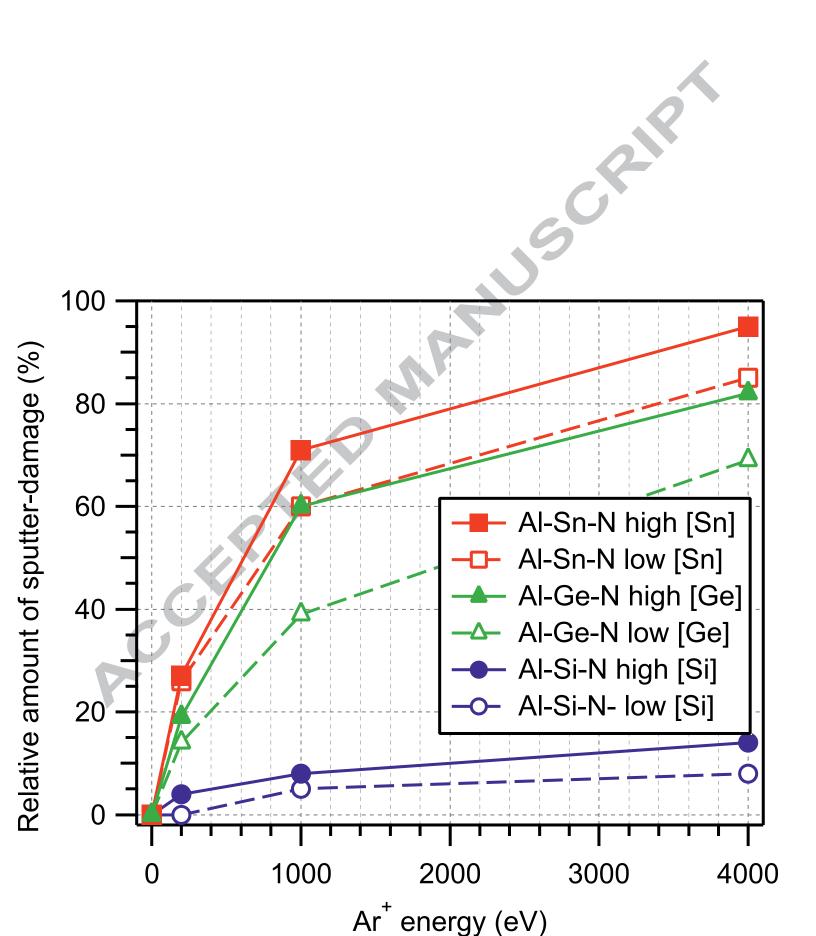


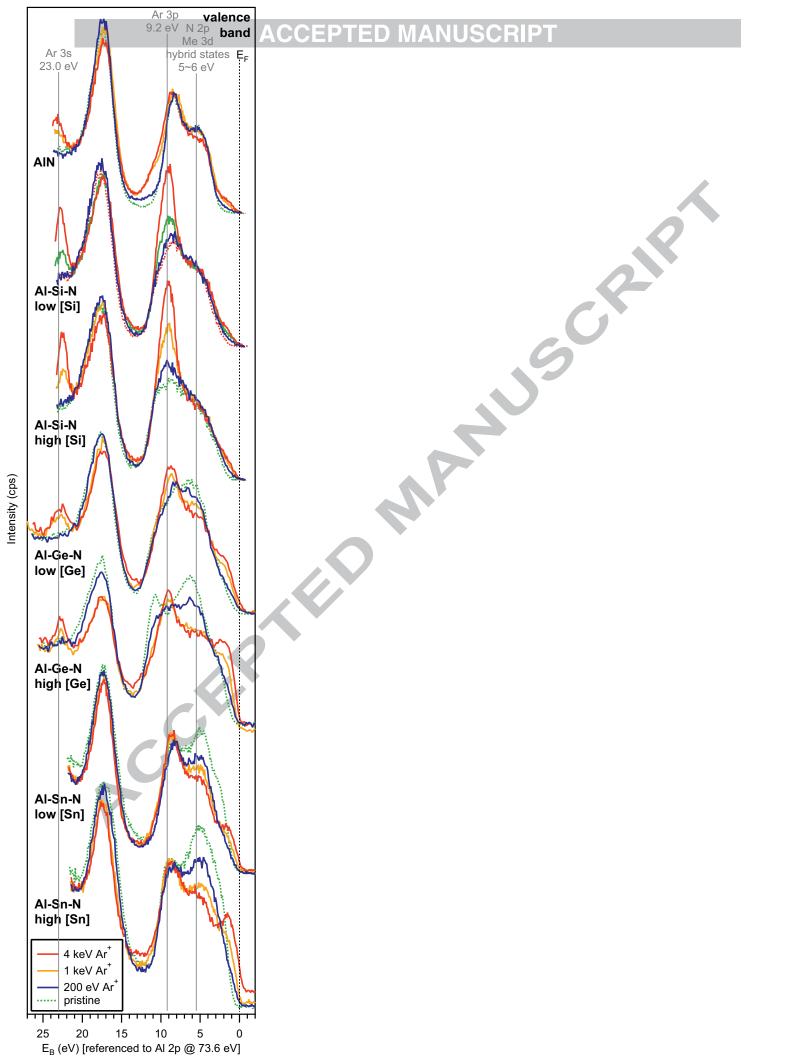


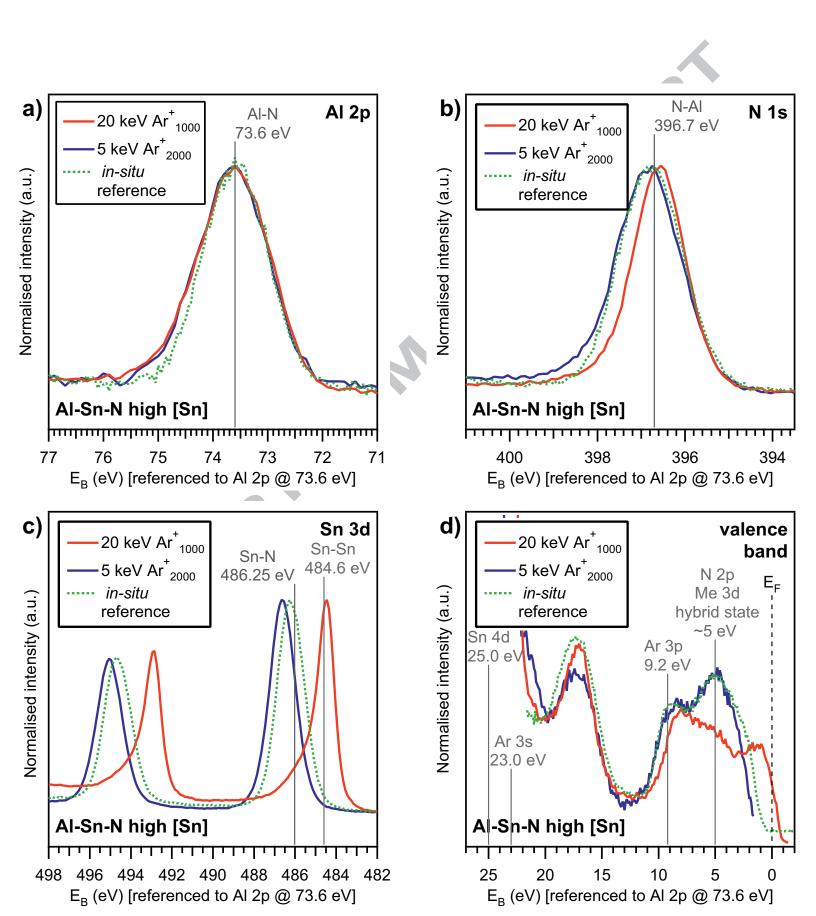
498 496 494 492 490 488 486 484 482 E_B (eV) [referenced to Al 2p @ 73.6 eV]

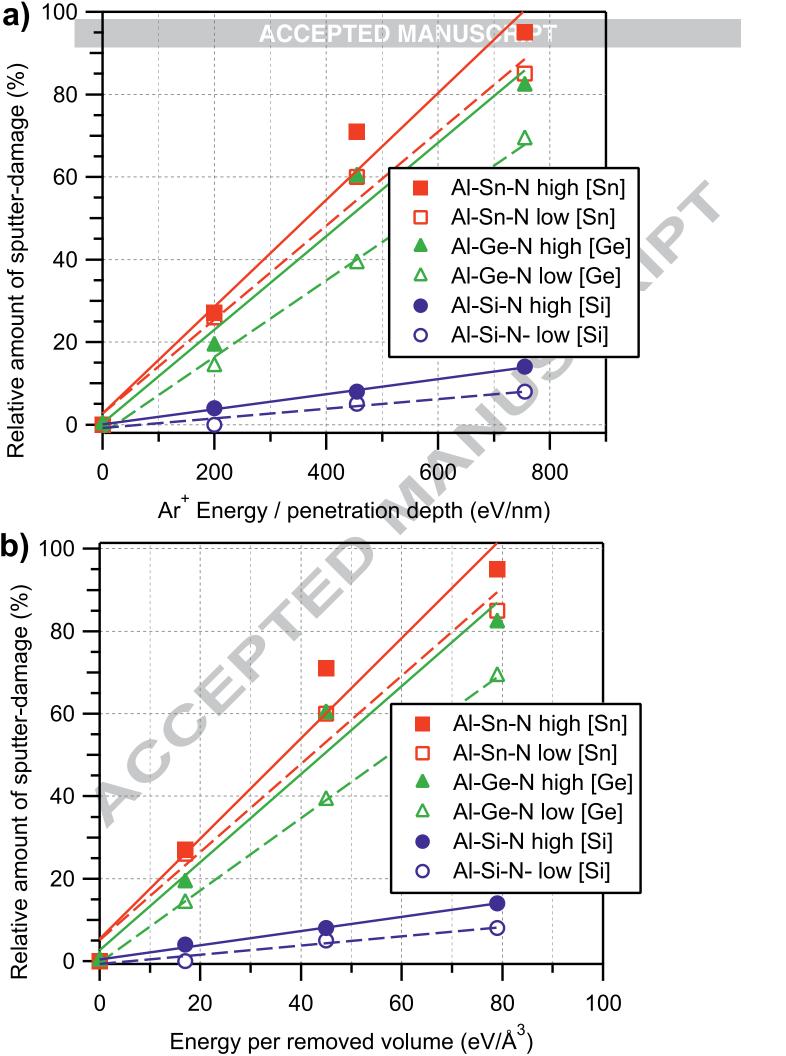


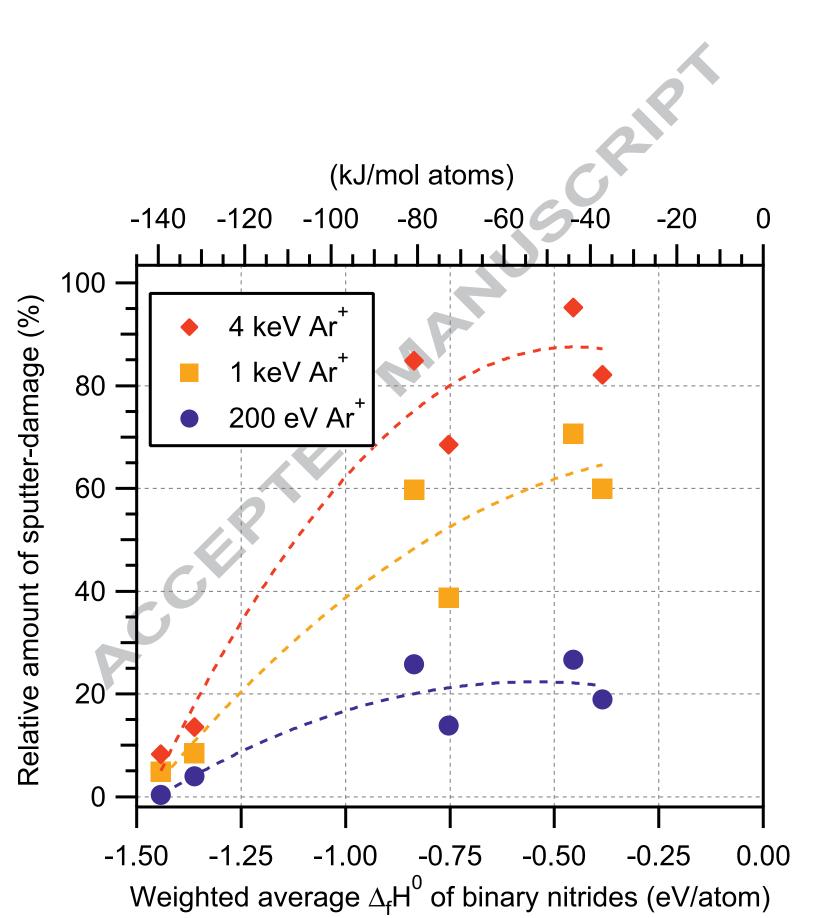
E_B (eV) [referenced to Al 2p @ 73.6 eV]

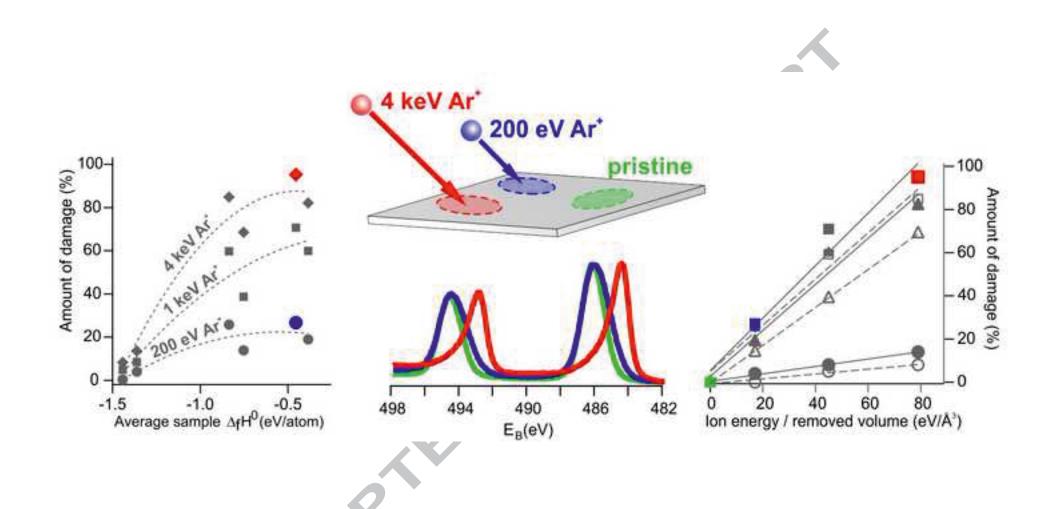












Highlights

- XPS analysis performed after different ion-etching methods
- Nitride coatings with different (meta)stability investigated
- Sputter-induced artefacts strongly dependent on material (average) formation enthalpy
- volum con beams Sputter-induced artefacts linearly dependent on energy deposited per removed volume