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CleanEx – A Versatile Automated Methane Preconcentration Device for High-Precision Analysis of ¹³CH₄, ¹²CH₃D, and ¹³CH₃D

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ABSTRACT: The relative abundance of methane isotopologues offers key insights into the global methane (CH₄) cycle. Advances in laser spectroscopy enable routine high-precision measurements even for rare deuterated methane isotopologues, ¹²CH₃D and ¹³CH₃D, provided there are sufficiently high methane amount fractions and reproducible measurement conditions, which can be achieved by CH₄ adsorption-desorption techniques. We present a new cryogen-free automated preconcentration device – CleanEx – designed for quantitative extraction of CH₄ from large volumes of sample gas and for cleaning by stepwise temperature-controlled desorption to separate interferant gases. We show that CleanEx has the capability to preconcentrate methane by almost 2000-fold from ~18 L of air. The performance is demonstrated in a range of methane amount fractions between 2 ppm (μmol mol⁻¹), which corresponds to the present-day ambient air, up to 1000 ppm, representative for close to source or process conditions. Advantages over existing devices are a significantly larger primary adsorption trap and a secondary cryo-focusing step, which ensures separation of methane from major atmospheric compounds, i.e., O₂, Ar, and CO₂. We have demonstrated quantitative extraction of methane, with no significant isotopic fractionation and high repeatability of 0.2‰, 0.6‰, and 0.8‰ (n=42) for the studied isotopologue ratios, ¹³CH₄/¹²CH₄, ¹²CH₃D/¹²CH₄, and ¹³CH₃D/¹²CH₄, during cryogenic adsorption-desorption on HayeSep D material. The developed device in combination with a suitable laser spectrometer offers a robust and autonomous method for precise continuous monitoring of δ¹³C-CH₄ and δD-CH₄ in ambient air and optionally Δ¹³CH₃D in process-derived methane.

Methane (CH₄) is both an important fossil and regenerative energy source and a potent greenhouse gas and air pollutant. This poses multiple research questions with respect to origin and conditions of formation in energy exploration^{1,2} but also in atmospheric budgeting.³ Isotope ratios ¹³C/¹²C and D/H measured through singly substituted ¹³CH₄ and ¹²CH₃D isotopologues are valuable tracers, which can help to distinguish the biogenic, abiotic, and thermogenic origins of methane (see, e.g., Menoud *et al.*⁴ and references therein). Analyses of doubly substituted (clumped) isotopologues ¹³CH₃D and ¹²CH₂D₂ provide independent constraints on formation temperature (for equilibrium processes), reaction mechanisms, mixing and destruction processes.^{2,5}

The main analytical challenge of methane isotopologues analysis is the requirement for high analytical accuracy, generally in the sub-per-mille range, at low relative abundances. Measurements of $^{13}\text{CH}_4/^{12}\text{CH}_4$ ratios are routinely performed with commercial tunable mid-IR laser direct absorption and cavity-ring down spectrometers at atmospheric abundances 6,7 while $^{12}\text{CH}_3\text{D}/^{12}\text{CH}_4$ analysis in ambient air requires precedent preconcentration. 8,9 In case of doubly substituted isotopologue analysis, there are currently two competing analytical techniques, both applied on pure or high-concentration samples: high-resolution isotope ratio mass spectrometry (HR-IRMS) 10,11 and quantum cascade laser absorption spectroscopy (QCLAS) $^{12-16}$. At the moment of writing, both methods are capable of achieving precision of better than 0.1% and 1% for $\Delta^{13}\text{CH}_3\text{D}$ and $\Delta^{12}\text{CH}_2\text{D}_2$, respectively.

Methane can be preconcentrated from ambient air or target process gases using cryogenic adsorption-distillation, making use of differences in boiling temperatures. Different high-volume, manual and liquid nitrogen¹⁷ or low-volume, automated, and cryogenfree^{18,19} devices have been realized and integrated into mass spectrometry workflows.²⁰ Laser spectroscopic analyses of deuterated ¹²CH₃D and ¹³CH₃D isotopologues pose distinct challenges with

respect to preconcentration, in particular the requirement for higher sample volumes, and the need for automated, cryogen-free operations to enable continuous lab or field operations. Published preconcentration devices, $^{8.9}$ however, are optimized for only 0.4-0.6 $\mu mol\ CH4$ from $5-7.5\ L$ of air and do not achieve preconcentration factors required for clumped isotope analysis. Besides, one-trap systems have shown difficulties with quantitative separation from oxygen. 8

In this study, we extend the performance of automated, cryogenfree preconcentration systems for laser spectroscopic analyses of rare CH₄ isotopologues. The objective of the further developments is twofold: (1) Enhance the preconcentration factor for CH₄ extraction from ambient air implementing a second cryo-focusing trap to improve separation of bulk gases and enable high-precision and accurate optical analysis of isotopologue ratios in ~1 μ mol CH₄ samples; (2) Enlarge the capacity of the preconcentration device to process $\geq 50~\mu$ mol CH₄ extracted from process-specific samples at elevated CH₄ mole fraction to enable optical Δ^{13} CH₃D analysis.

EXPERIMENTAL SECTION

The Cleaning and Extracting unit presented in this technical note CleanEx is a further development in a family of fully automated cryogen-free Trace gas Extractors (TREX) designed for nitrous oxide²¹ and methane⁸ extraction from ambient air and subsequent isotope analysis with a laser spectrometer. TREXs shared a common design platform equipped with a detachable trap and gas flow scheme inherited from Medusa,²² and are fully automated by a customized LabView (National Instruments, USA) code developed for autonomous operation. The main upgrade of the new unit with respect to the previous generation is threefold: (1) a 50% enlarged amount of adsorbent in the primary trap, (2) a lower operating temperature of the primary trap (T1) at -171°C, and (3) a secondary cryo-focusing trap (T2). With these modifications, we address a

major limitation of the previous TREX unit, 8 namely, an elevated oxygen content in the processed sample. The latter leads to an offset in $\delta^{13}\text{C-CH}_4$ measurements due to the induced matrix effect, which has to be characterized and post-corrected. 23 Complete removal of oxygen thus significantly simplifies the instrument's calibration and correction scheme.

Method Overview. The basic principle of methane extraction and purification is based on the separation of air constituents by their boiling point temperatures. Stepwise temperature control of the absorbent combined with flushing of the absorbent-filled traps by a carrier gas allows separation of methane (boiling point,

−161.5 °C; mole fraction in dry ambient air, 1889±2 ppb)²⁴ from major dry air compounds with a lower boiling point, i.e., N₂, O₂, Ar, CO, and trace gases with a higher boiling point, i.e., Kr, N₂O, CO₂.

It is critically important for isotope analysis to minimize changes in isotopologue ratios, called fractionation effects, which is generally ensured by quantitatively complete recovery of the methane fraction. Therefore, significant effort has been invested toward optimization of the cooling and heating cycles of the traps, the choice of carrier gas flows, and the optimal timing of sample refocusing from T1 to T2.

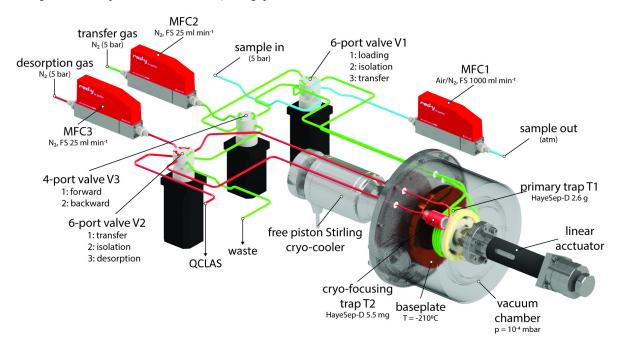


Figure 1. Simplified depiction of the CleanEx flow layout for methane preconcentration and introduction into a QCLAS device. Multiport valve V1 controls the sample flow through the primary trap (T1) or isolates the trap. V2 changes the flow direction (forward vs backward) through T1. V3 controls the sample transfer onto the cryo-focusing trap (T2) by connecting the traps in series, or isolates T2. Mass flow controllers MFC1-3 regulate the flows of the sample, transfer, and desorption gas, respectively. The stainless-steel vacuum chamber, shown transparent for clarity, is evacuated with a turbo-molecular pump to avoid condensation on the cooled parts.

Preconcentration Unit Design and Operation. The primary trap (T1, light green colored coil in Figure 1) is made of an electropolished stainless-steel tube (3 mm i.d., 4 mm o.d., total length 1 m) twisted in a coil (3.5 turns) around an aluminum standoff (80 mm o.d.). The middle part (85 cm) of the coil is filled with 2.6 g of the HayeSep D porous polymer adsorbent (Sigma-Aldrich, Merck KGaA, Germany). Glass wool insertions (20 mm on both sides) and mesh wire insertions (50 mm at the entrance and 25 mm at the exit) mechanically retain the adsorbent, cool the gas, and partially adsorb gases with higher boiling points, e.g., CO₂ and N₂O. The standoff is mounted on a linear actuator contacted with a wave spring, which ensures even and adjustable force distribution between standoff and baseplate. Rapid cooling of the trap is achieved by pressing the standoff against the massive copper baseplate (diameter 14 cm, thickness 1 cm). The temperature of the baseplate is maintained at -215°C by a free-piston Stirling cryocooler (capacity 10 W, CryoTel GT, Sunpower, Inc., USA), monitored by a Type-K thermocouple. The heat sink of the cryocooler is stabilized at 18°C by a liquid recirculating chiller (ThermoRack 801, SolidState Cooling Systems, USA). Good thermal contact is ensured by polishing the baseplate (roughness 0.2 µm) and standoff surfaces and by applying a thin layer of thermo-conductive paste (340 HSC, Dow Croning, USA). For desorption and conditioning, T1 is detached from the baseplate and heated by a polyamide heating pad (Minico Products, Inc., USA). The trap temperature is monitored with a Pt-102 sensor inserted into the standoff body and precisely

controlled using a PID controller (diraTron, Jumo AG, Switzerland). PID parameters were optimized to stabilize the temperature of the trap around -171°C and to provide rapid heating to target temperatures, yet to prevent overshoot.

A cryo-focusing trap (T2, red colored coil in Figure 1) made of a 1/16 in. o.d stainless steel tube and containing 5.5 mg of HayeSep D is coiled (seven turns) onto a 17 mm thin-walled stand-off. The temperature of T2 is monitored by a Type-E thermocouple and resistively heated applying high current (7.5 A), using custom-made electronics, regulated by a PID controller (diraTron, Jumo AG, Switzerland).

T1 and T2 are integrated in the instrument's flow layout as shown in Figure 1. Six-port valves V1 and V2 (Valco Instruments Inc., Switzerland) are installed to regulate gas flows toward T1 and T2, respectively, and isolate the traps during cooling phases. The four-port valve V3 (Valco Instruments Inc., Switzerland) regulates the flow direction through T1. Three mass flow controllers MFC1-3 (Red-y Smart Series, Vögtlin Instruments, Switzerland, calibrated at 20°C) are deployed for reproducible and precise flow control of the sample gas (MFC1, full scale 1000 mL min $^{-1}$), and transfer as well as desorption gas N $_2$ (MFC2-3, full scales 25 mL min $^{-1}$).

The operation sequence and parameter settings were optimized to ensure quantitative adsorption on the primary trap, complete desorption of methane from T1 and refocusing on T2, and efficient elution from T2. An exemplary preconcentration cycle is presented in Figure S1 together with a description of major operation phases.

RESULTS AND DISCUSSION

Versatile operation of the preconcentration device CleanEx relies on several factors: sufficient adsorption capacity to process required amounts of methane, effective separation of methane from other sample gas constituents to avoid spectral interferences and matrix variation induced errors, desirable enhancement in CH₄ concentration between input and output samples to match the operation requirements of the laser spectrometer, and finally, reproducible operation with quantitative isotopologue extraction to avoid or minimize isotopic fractionation. These factors were extensively studied as presented in the following sections.

Adsorption Capacity. One of the design criteria for the presented setup compared to earlier versions and solutions realized for IRMS analysis was to enhance and test its capability to process large amounts of CH₄ suitable for analysis of clumped isotopes by QCLAS. The total amount of CH₄ that can be processed by CleanEx is limited by the maximum sample volume processed before CH₄ exits the primary trap, named adsorption capacity. If further cleaning of the CH₄ sample is required, readsorption on T2 has to be tested as well. Preliminary experiments indicated that the adsorption capacity for CH₄ is a function of trap temperature, sample flow rate, and CH₄ concentration in the sample gas.

In a specific set of experiments, the adsorption capacity of the primary trap was tested at three trap temperatures below the boiling point of methane (-166, -171, -176°C) and three sample flow rates (500, 700, 900 mL min⁻¹) for CH₄ concentrations typical for ambient air (2.0 ppm of CH₄ in whole air) and process-level (1000 ppm of CH₄ in synthetic air) applications. The tested lowest trap temperature (-176°C) and highest flow rate (900 mL min⁻¹) represent threshold values for T1 in the current CleanEx configuration.

Results presented in Figure 2A indicate a strong increase of the adsorption capacity with lower trap temperatures and a weaker, inconsistent dependence on the flow rate at ambient CH₄ mole fractions. One should keep in mind, however, that the indicated trap temperature represents the actual temperature at the sensor location but not the temperature inside the tubing, i.e. where gas molecules are actually adsorbed. This might explain the fact, that for a given trap temperature (e.g., -176°C) at high flow rates the adsorbed volumes of oxygen and nitrogen are lower (160 mL at 900 mL min $^{-1}$ and 214 mL at 500 mL min $^{-1}$, respectively). At any temperature of T1 CleanEx is capable of extracting more than sufficient amounts (1.5 μ mol) of CH₄ from air required for precise δ D-CH₄ analysis by a dual laser QCLAS (Aerodyne Research, Inc.) requiring 0.5 μ mol CH₄.^{8,9}

The adsorption capacity of the primary trap shows little dependence on the CH₄ amount fraction in the sample. In a wide range of mole fractions between 2 and 1000 ppm, the adsorption capacity was above 17 L, when the trap temperature was set to -176°C and the flow of the sample was 900 mL min⁻¹. At a very high methane mole fraction of 2% in a synthetic air matrix, the adsorption capacity was still 11 L under the same experimental conditions. Consequently, at CH₄ amount fractions in the sample gas of 1000 ppm or even at percent levels, typical for process applications, sufficient CH₄ for precise analysis of $\Delta^{13}\text{CH}_3\text{D}$ (50 µmol) and even $\Delta^{12}\text{CH}_2\text{D}_2$ (500 µmol) can be preconcentrated.

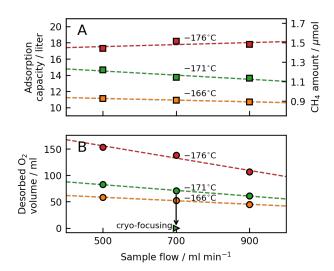


Figure 2. (A) Adsorption capacity of the primary trap for sample gas with ambient concentrations and corresponding methane amount. (B) total volume of oxygen desorbed from T1 (circles) for different trap temperatures as a function of sample flow rate and for one exemplary flow rate after cryo-focusing on T2 (triangle). Dashed lines are linear interpolations.

Depending on the specific application, a second cryo-focusing step on T2 of CleanEx might be required, for example, to quantitatively separate O2 from an ambient air matrix. T2 was designed as a permanently attached (nonmoveable) trap. For pure CH4 samples, T2 was capable to adsorb 15±2 mL at 5 mL min⁻¹ flow rate. For cryo-focusing of methane extracted from ambient air or process gases and desorbed from T1, CH4 is accompanied by coadsorbed gases (mainly, N2, O2), which limits the adsorption capacity of T2. Quantitative CH₄ transfer and readsorption on T2 were demonstrated for ambient air even at high sample volumes (18 L STP). Efficient transfer is only possible when the exit of T2 was blocked for the initial phase of transfer. This prevents intrusion of ambient air which would otherwise contaminate and heat the trap due to adsorption of atmospheric gas compounds. For process-level CH₄ input concentrations, systematic tests with CH₄ amounts of 0.5-10 mL (STP) and trap temperatures of $T_{T1}=0^{\circ}\text{C}$ and $T_{T2} = -186$ °C display that breakthrough of T2 happens after a 5 min transfer with a 5 mL min⁻¹ N₂ flow for any sample larger than 1.5 ml CH₄. This indicate that with the current T2 design sufficient CH₄ (67 μ mol, 1.5 mL STP) for precise Δ ¹³CH₃D analysis by QCLAS can be quantitatively readsorbed. For precise analysis of Δ¹²CH₂D₂, the current capacity of T2 seems to be insufficient and would have to be replaced by a larger cryo-focusing trap. In the dual trap configuration presented in this study, we achieve 2000 - fold enhancement for ambient air samples of 15 L. The calculation of enhancement factors is presented in eq. S1 Supporting Information S3.

Separation Efficiency. A major limitation of existing preconcentration devices is the insufficient separation of bulk air constituents (e.g., O₂, Ar, Kr) having boiling point temperatures close to CH₄. Variations in the amount fractions of bulk air constituents affect the pressure broadening of the analyzed CH₄ lines, limiting the accuracy of optical analyzers.⁸ This effect is highly relevant for He and Ar, since their broadening coefficients are very different from nitrogen,²⁵ and to a lesser extent for krypton, whose broadening coefficient is very similar to that of nitrogen.²⁶ Therefore, one stimulus for the dual trap design of the CleanEx device was the urge for quantitative separation of O₂. Since we use high-purity nitrogen as a transfer and desorption gas, coadsorption of N₂ does not affect the gas matrix composition.

Oxygen coadsorption on T1 was systematically tested for different trap temperatures (-166, -171 and -176°C) and sample flow

rates (500, 700, 900 mL min⁻¹) along with the determination of CH4 adsorption capacity described before. For this, the O₂ amount fraction at the outlet of T1 was monitored during desorption with a paramagnetic analyzer (570A, Serovemex, UK) and the desorbed O₂ volume calculated as an integrated flow through the mass flow controller installed downstream of the primary trap. Results presented in Figure 2B indicate that higher amounts of O₂ are coadsorbed at lower T1 temperatures and lower adsorption flows, with the latter being rationalized by lower effective temperatures of the HayeSep D adsorbent. Partial removal of coadsorbed gases was accomplished implementing a stepwise heating profile of T1 (Figure S1C) before transfer of CH₄ and remaining coadsorbed gases on T2.

To monitor the selectivity of the complete two trap process for CH₄ separation, the bulk gas composition (O₂, Ar, Kr) of the gas matrix after desorption from T2 was analyzed by mass spectrometry (QMS, Vision 1000-C, MKS Instruments, Inc., USA). Concentration profiles of the desorbed gases (Figure S1E) demonstrate that no significant coadsorption of O₂ (< 0.5%) and Ar (< 0.02%) occurs. Krypton, however, which has a boiling point of only 8°C higher than methane and a mixing ratio of ~1 ppm in the atmosphere, is coeluted with CH₄, and cryogenic separation remains very challenging.

Isotopic Fractionation and Repeatability. An important characteristic of a preconcentration device for subsequent isotope analysis is the absence or at least constancy of changes in the isotopic composition of the target substance between input and output samples.

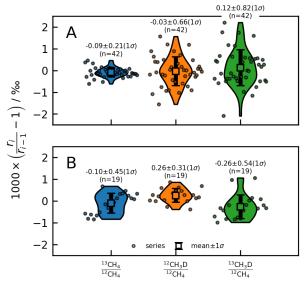


Figure 3. (A) Reproducibility of isotopologue ratio measurements for subsequent dual trap preconcentration cycles. (B) Magnitude of isotopic fractionation associated with methane extraction.

In the first step, we quantified the reproducibility of isotopologue ratios for 42 subsequent preconcentration cycles for a gravimetrically prepared 1000.4 ($\pm 1\%$ rel.) ppm of CH₄ in a N₂ mixture. In this experimental series (Figure 3A), each desorbed sample acted as a reference point for the following sample. Standard deviations of 0.2‰, 0.7‰ and 0.8‰ were determined for $^{13}\text{CH}_4/^{12}\text{CH}_4$, $^{12}\text{CH}_3\text{D}/^{12}\text{CH}_4$, and $^{13}\text{CH}_3\text{D}/^{12}\text{CH}_4$, respectively, resulting in the respective standard errors (1 S.E., n = 42) of 0.03‰, 0.11‰, and 0.12‰. The demonstrated high reproducibility ensures a close link between reference and sample measurements, when using an identical treatment approach, i.e., preconcentration of both gases. However, this experiment is insensitive to the presence of isotope fractionation effects, which we quantified in another set of extractions described below. The average recovery yield was determined from the CH₄ amount adsorbed on and desorbed from T1 in a separate

experiment, which confirmed the quantitative recovery (99 \pm 2%, n = 42).

In the second experiment, we estimated the magnitude of isotope fractionation in a series (n = 19) of extraction cycles, when the inhouse working reference (δ^{13} C_{VPDB} = -44.21 ± 0.15 %, δ D_{VSMOW} = $-189.0\pm1\%$, 99.9995% CH₄) was dynamically diluted with N₂ in a 1:1000 ratio (1000 ppm of CH₄) before being processed by CleanEx. Figure 3B shows isotopologue ratios analyzed by QCLAS in the processed sample referenced to the undiluted / unprocessed CH₄ in N₂ gas. Details on QCLAS performance are given in Supporting Information S2. The effect of differences in CH₄ amount fractions on isotopologue ratios was corrected (Table S1). The mean observed deviations of -0.1%, 0.3%, and -0.3% for δ^{13} C-CH₄, δ D-CH₄, and δ^{13} CH₃D, respectively, are within one standard deviation of the measurements, which indicates that fractionation effects are not significant. In comparison with the previously reported preconcentration devices capable of direct deuterated methane measurements, we have achieved almost twofold improvement in uncertainty for ¹²CH₃D/¹²CH₄ and for the first time demonstrated the capability for doubly substituted clumped ¹³CH₃D analysis.

CONCLUSION

We have developed and characterized a fully automated cryogen-free preconcentration unit to enhance the mole fraction of methane by a factor of 2000 from the ambient level and enable precise and accurate laser spectroscopic analysis of ¹²CH₃D in ambient methane. The maximum amount of methane that can be processed in a two-trap configuration from process level concentrations (1000 ppm of CH₄) is as high as 0.67 mmol (1.5 mL STP). This amount is sufficient to enable direct high-precision analysis of doubly substituted (clumped) isotopologue ¹³CH₃D. Quantitative and reproducible methane recovery without significant fractionation effects for isotopologue ratios ¹³CH₄/¹²CH₄, ¹²CH₃D/¹²CH₄, and ¹³CH₃D/¹²CH₄ has been demonstrated in this study. The developed device can be adapted for analysis of other rare isotopic species.

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SUPPORTING INFORMATION

The Supporting Information is available free of charge at https://pubs.acs.org/doi/10.1021/acs.analchem.2c01949

Exemplary preconcentration unit operation cycle with detailed description of each phase; statement on the performance of QCLAS; mathematical calculation of enhancement factor; traps breakthrough measurement protocol. Data underlying the results presented in this paper is available online.²⁷

AUTHOR CONTRIBUTIONS

Ivan Prokhorov optimized and tested the preconcentration device, designed and conducted laboratory experiments, and analyzed the data. Joachim Mohn conceptualized and supervised the project, and

discussed the results. The manuscript was written with contributions of both authors. Both authors have given approval to the final version of the manuscript. The authors declare no competing financial interest.

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